

ON CHIP PHOTONIC INTERCONNECTIONS: WIRED AND WIRELESS TECHNOLOGIES

Prof. Giovanna Calò, Politecnico di Bari

Prof. Gaetano Bellanca, University of Ferrara

Ring-Based Networks for On Chip Optical Interconnections:
from device design to fabrication and final characterization

- Describe our work on Optical Network on Chip (ONoC) from waveguide-based topologies to wireless solutions

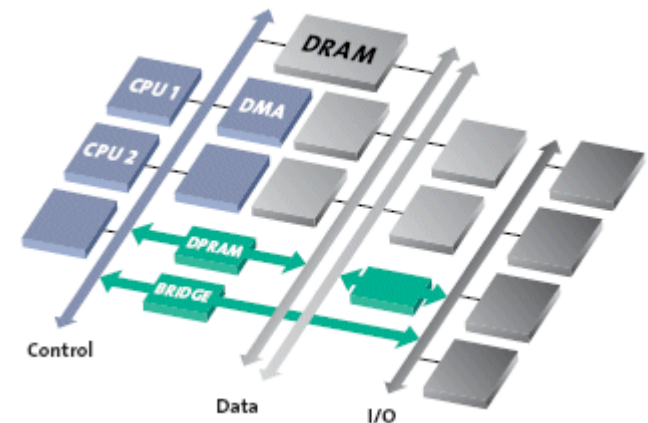
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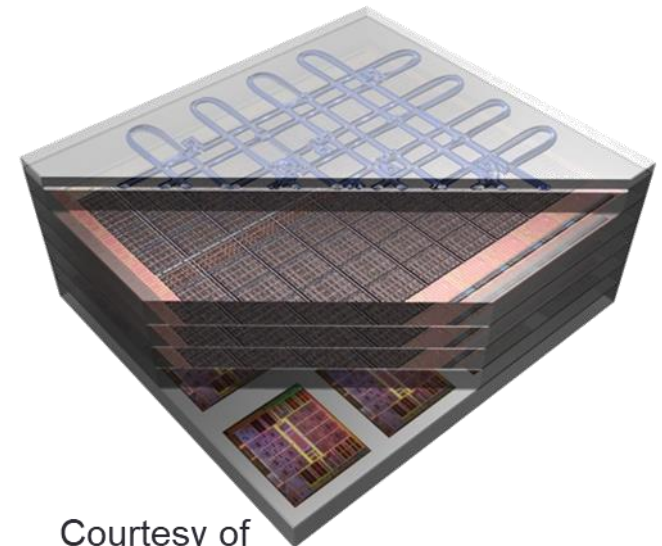
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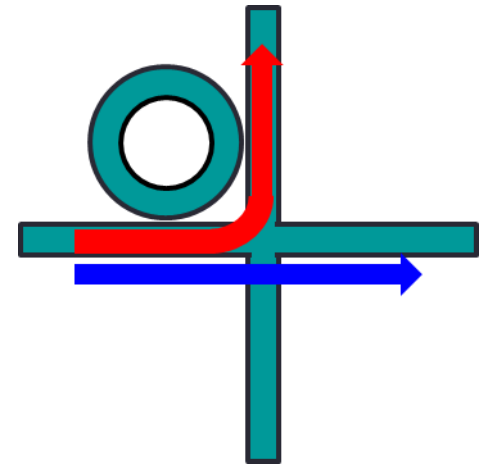


Courtesy of
Columbia University

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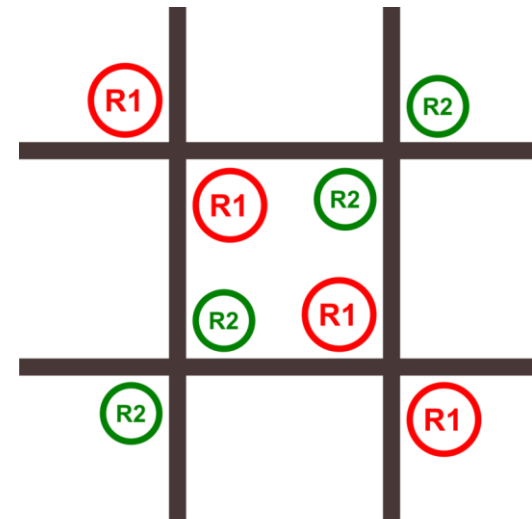
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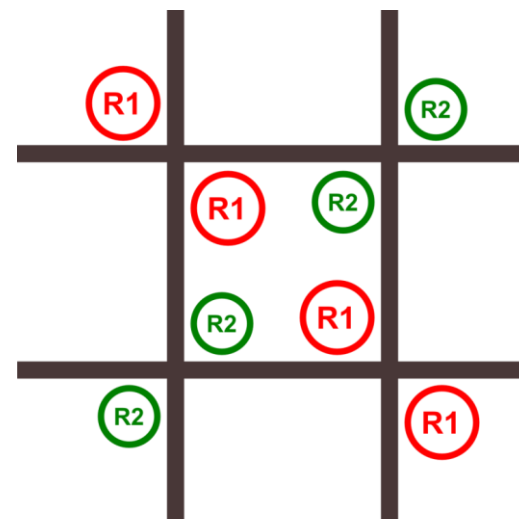
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- Simple network (GWOR).
Problems and Performance
Evaluation



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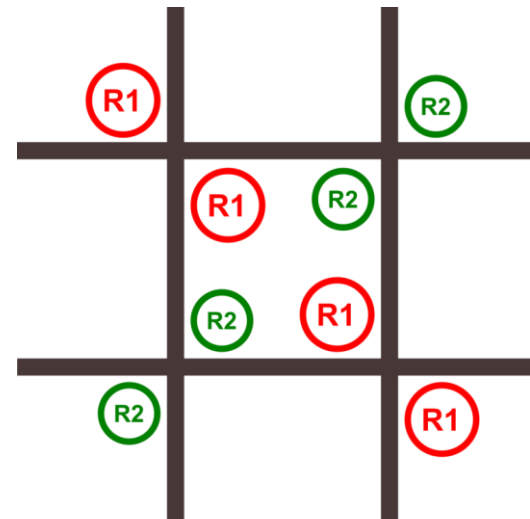
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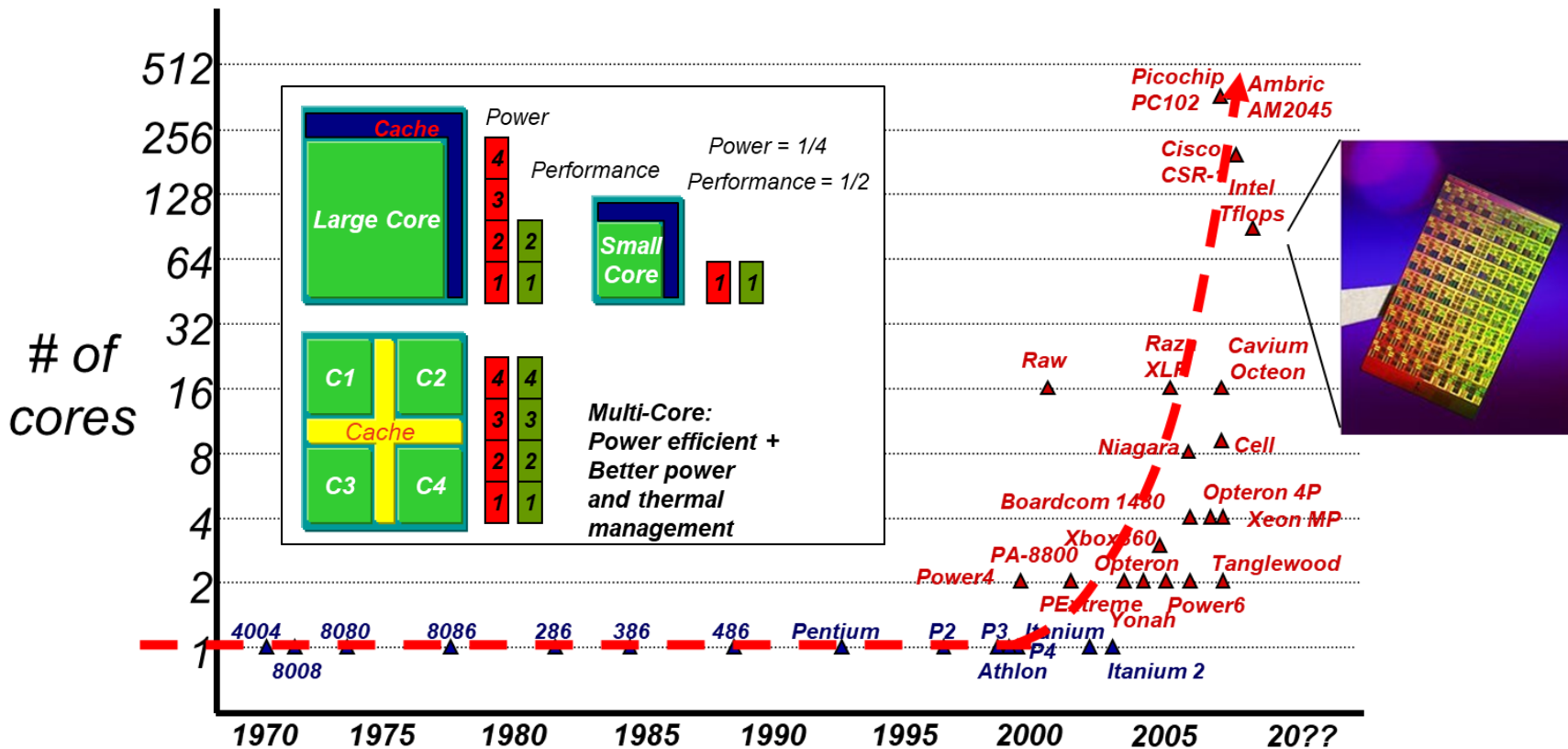
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- Introduction and motivations for electrical NOC and ONoC
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- Conclusions



- Our interest in Optical Network on Chip is dated 2010



- Every commercial manufacturer of High-Performance Processors was introducing products based on Multi-Core Architectures

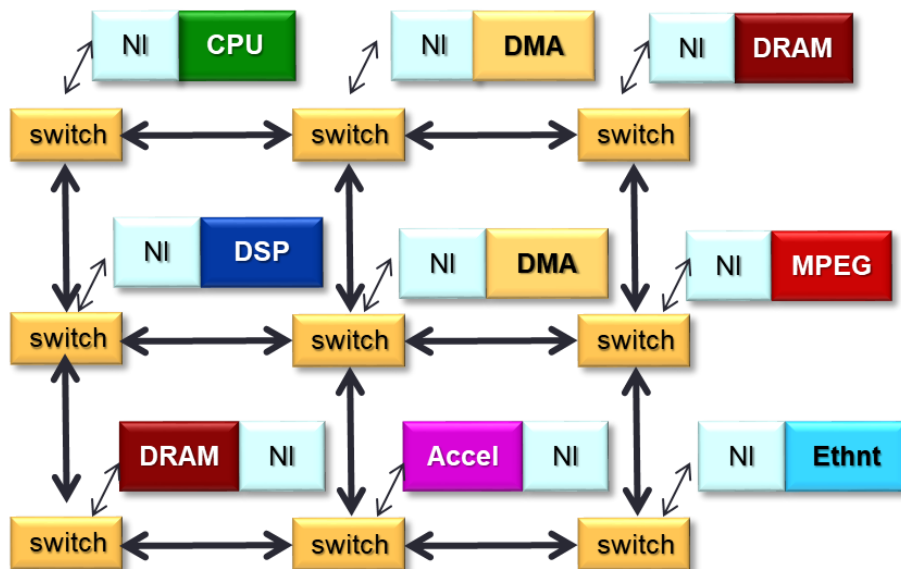
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- The Communication Bottleneck



- SERIALIZATION of bus access requests
- Single outstanding transaction allowed
- If wait states are needed, everybody waits

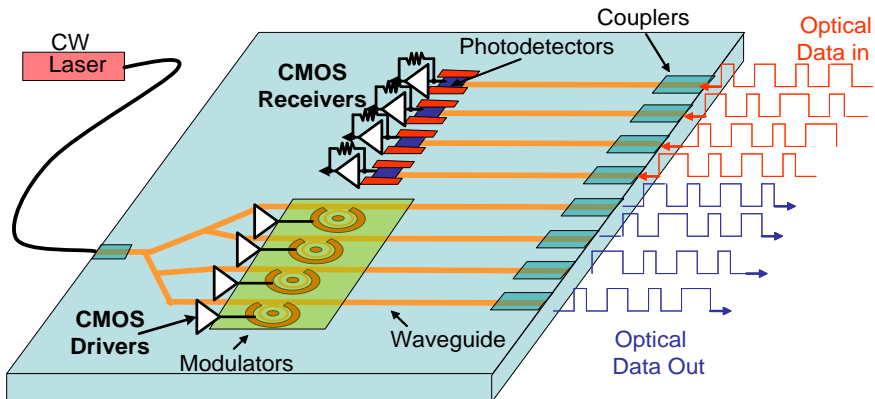
- A possible answer: Network-on-Chip (NoC)



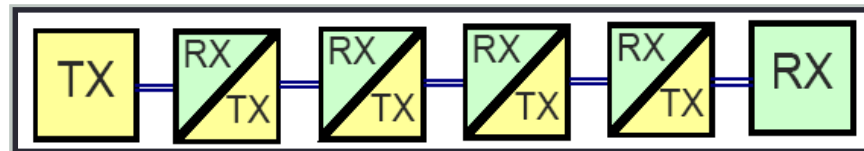
- High heterogeneity/flexibility
 - Cores will operate at different frequencies, data widths and protocols
- High performance (bandwidth - latency)
 - Many cores will want to communicate, simultaneously
- Short and structured wiring
 - Point-to-point, predictable routing

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• Changing Technology? On-Chip Optical Links

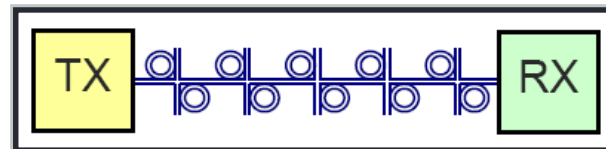


NoC

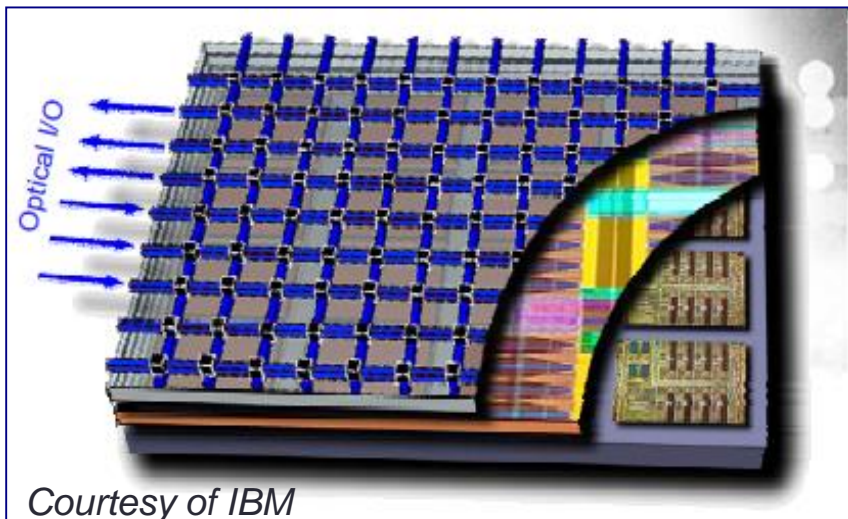


- Power is Bandwidth \times Length dependent
- Buffering, Receiving and Retransmitting
- Power-hungry and BW limited by pin count

ONoC



- Power independent of Bitrate and Length
- Modulate/Receive high BW data stream once – no retransmit
- Almost seamless scaling to multi-chip systems
- Broadband switching fabric nearly free in power dissipation (scalability)



Courtesy of IBM

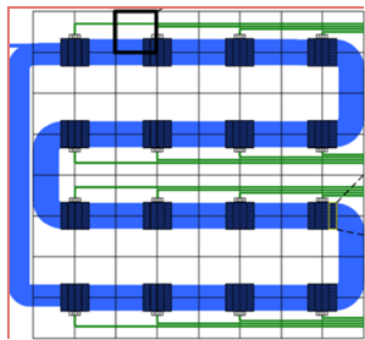
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- Network Proposals

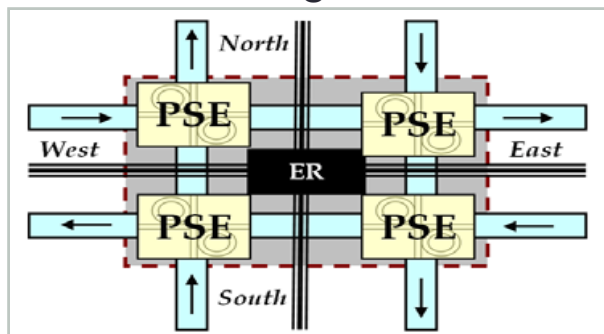
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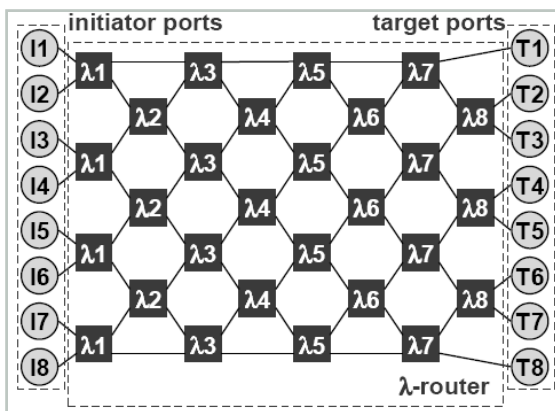
Photonic Crossbar



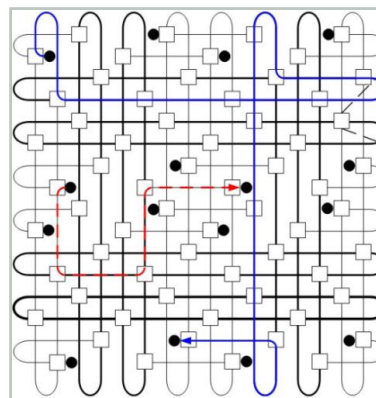
Blocking Switch



Passive Network



Folded Torus

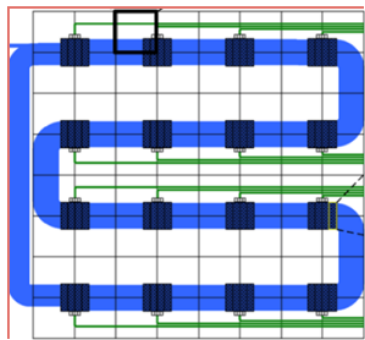


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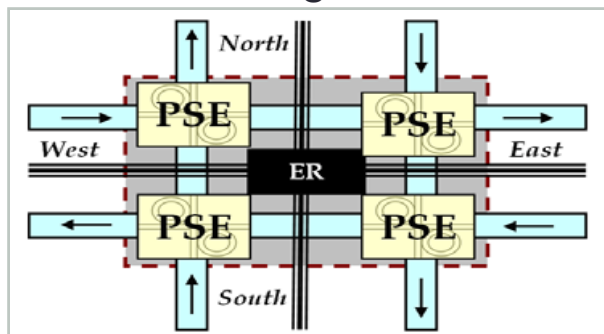
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All based on Ring Resonators

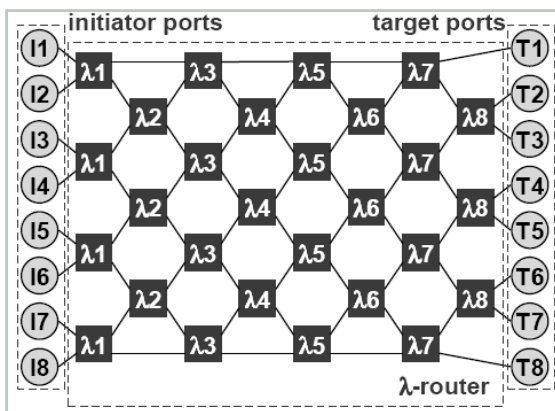
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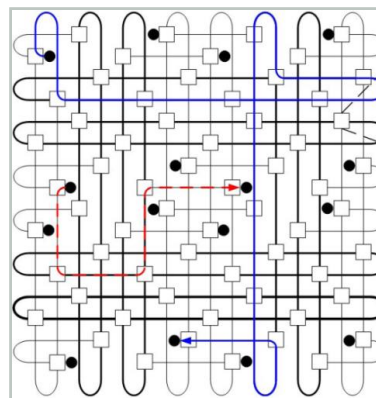
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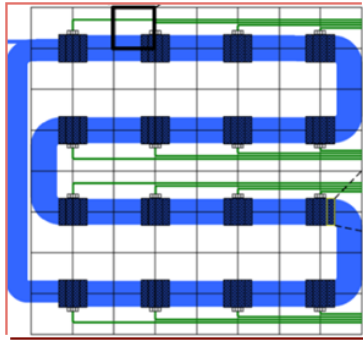


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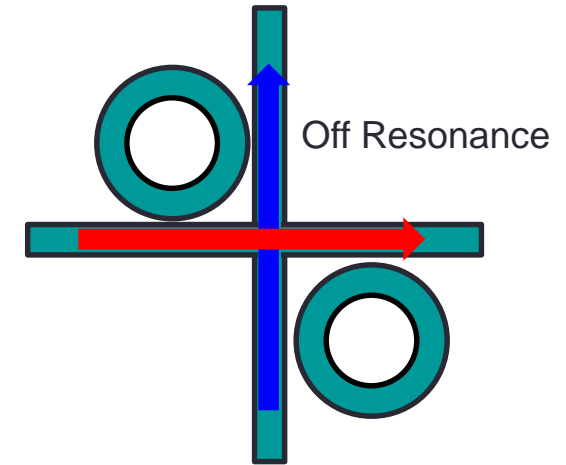
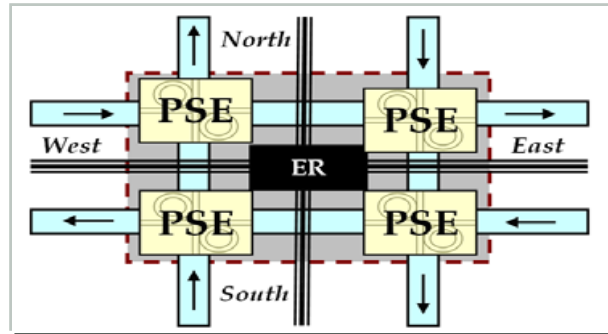
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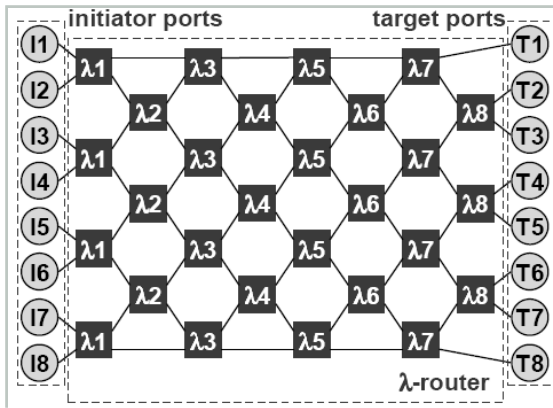
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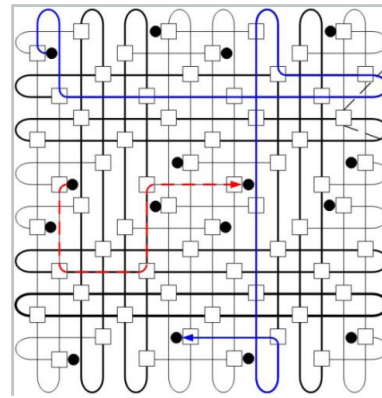
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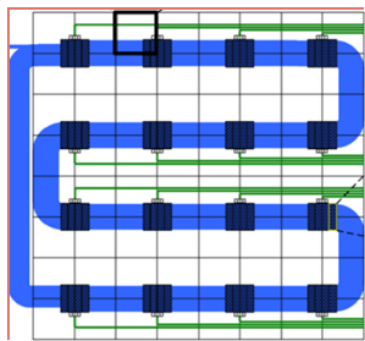
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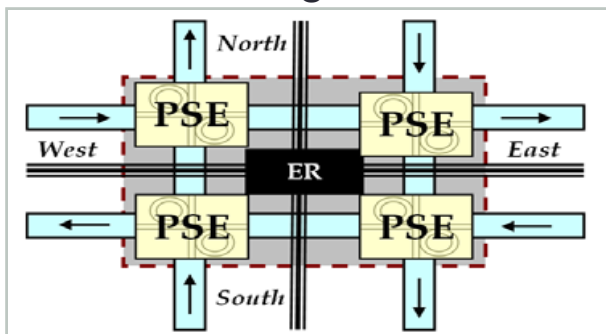
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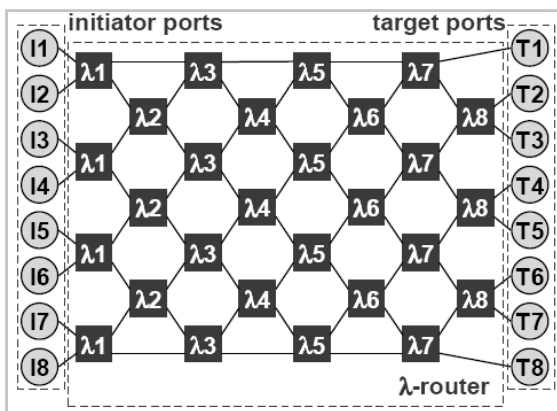
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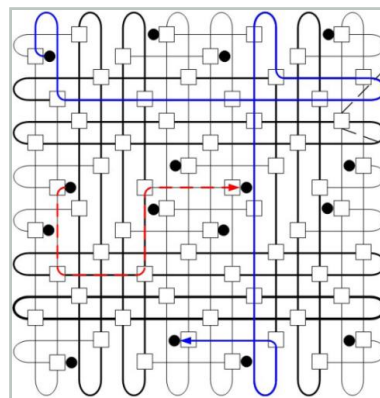
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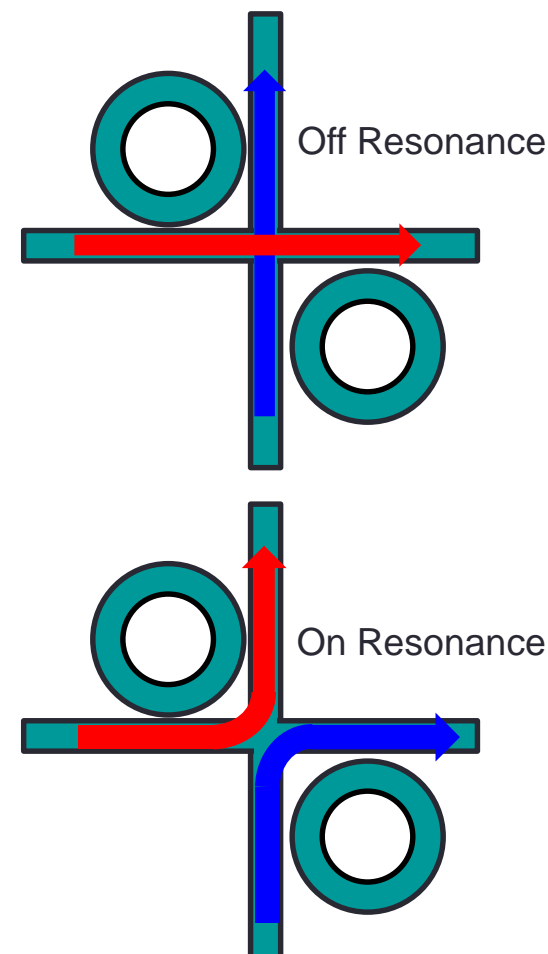
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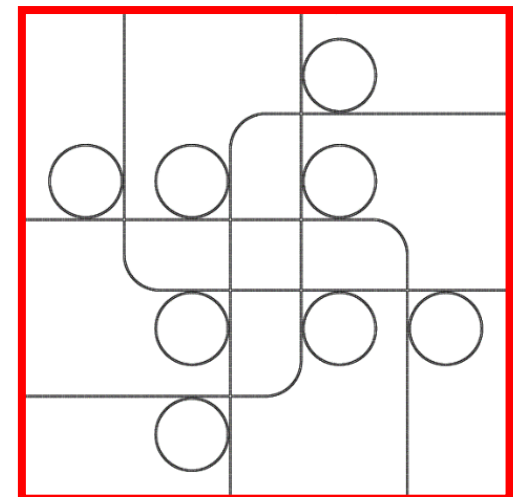
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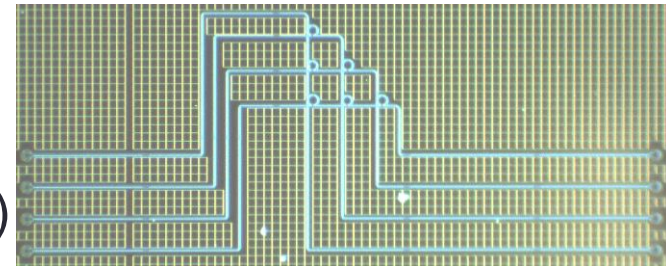
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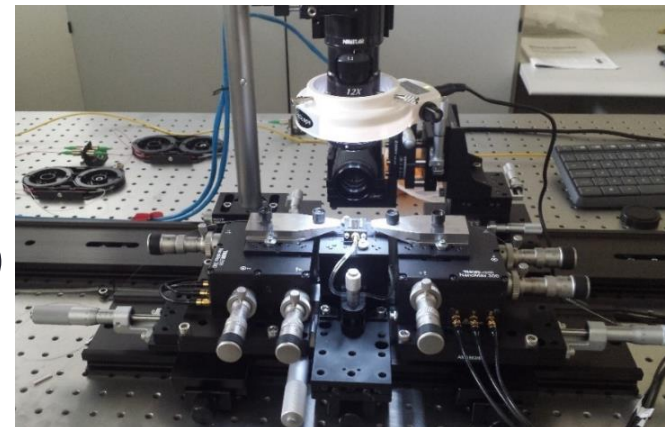
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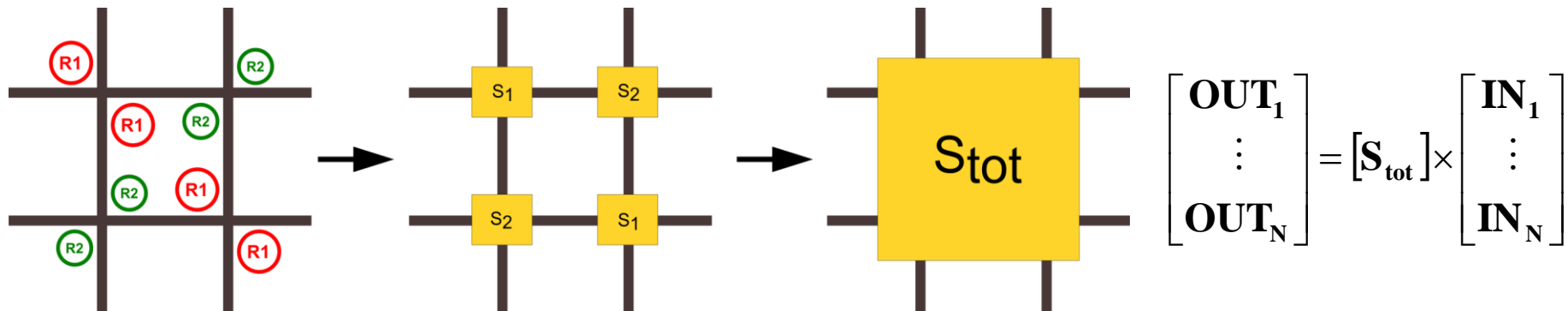
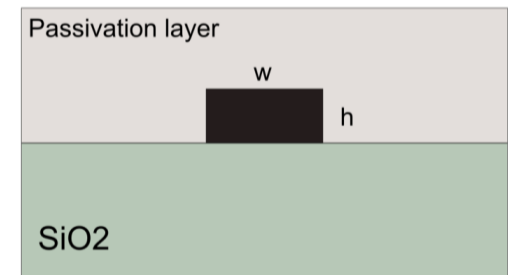
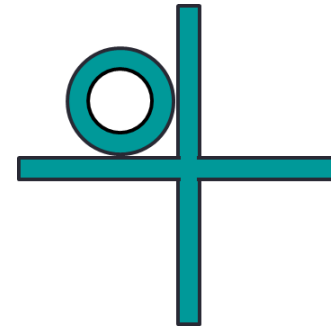
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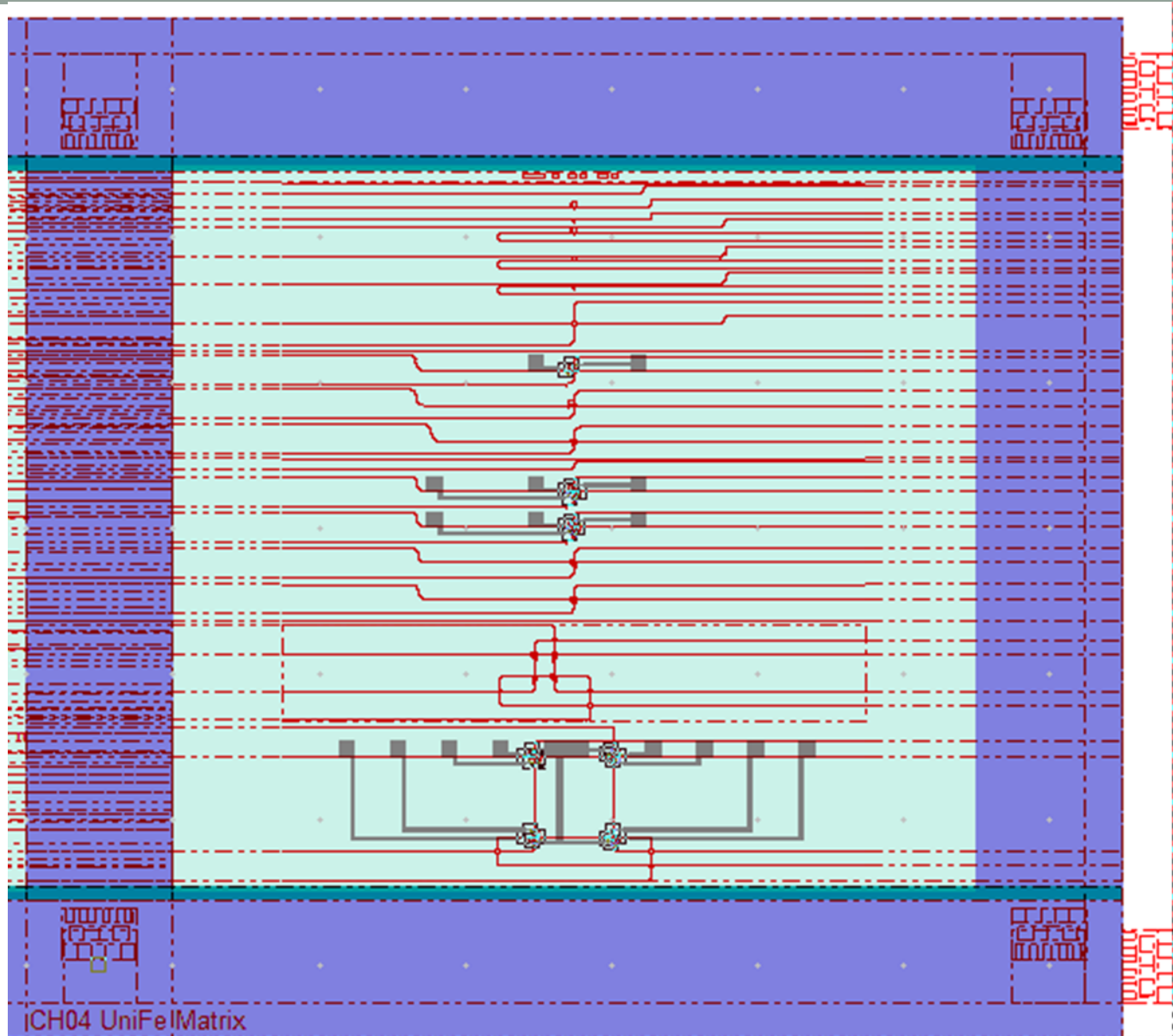
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 - Characterization of the fabricated devices



- Photonic Switching Element based on Ring Topology
- Silicon on Insulator (SOI) Technology
 - SOI waveguides 480×220 nm (h \times w)
 - Rings Radius = 18/20 μ m
- Simulation Tools
 - FDTD for Device Analysis
 - S-Matrix for Circuit Level Modeling
 - The networks are modeled as an incremental composition of BLACK BOX described via the Scattering Matrix formalism

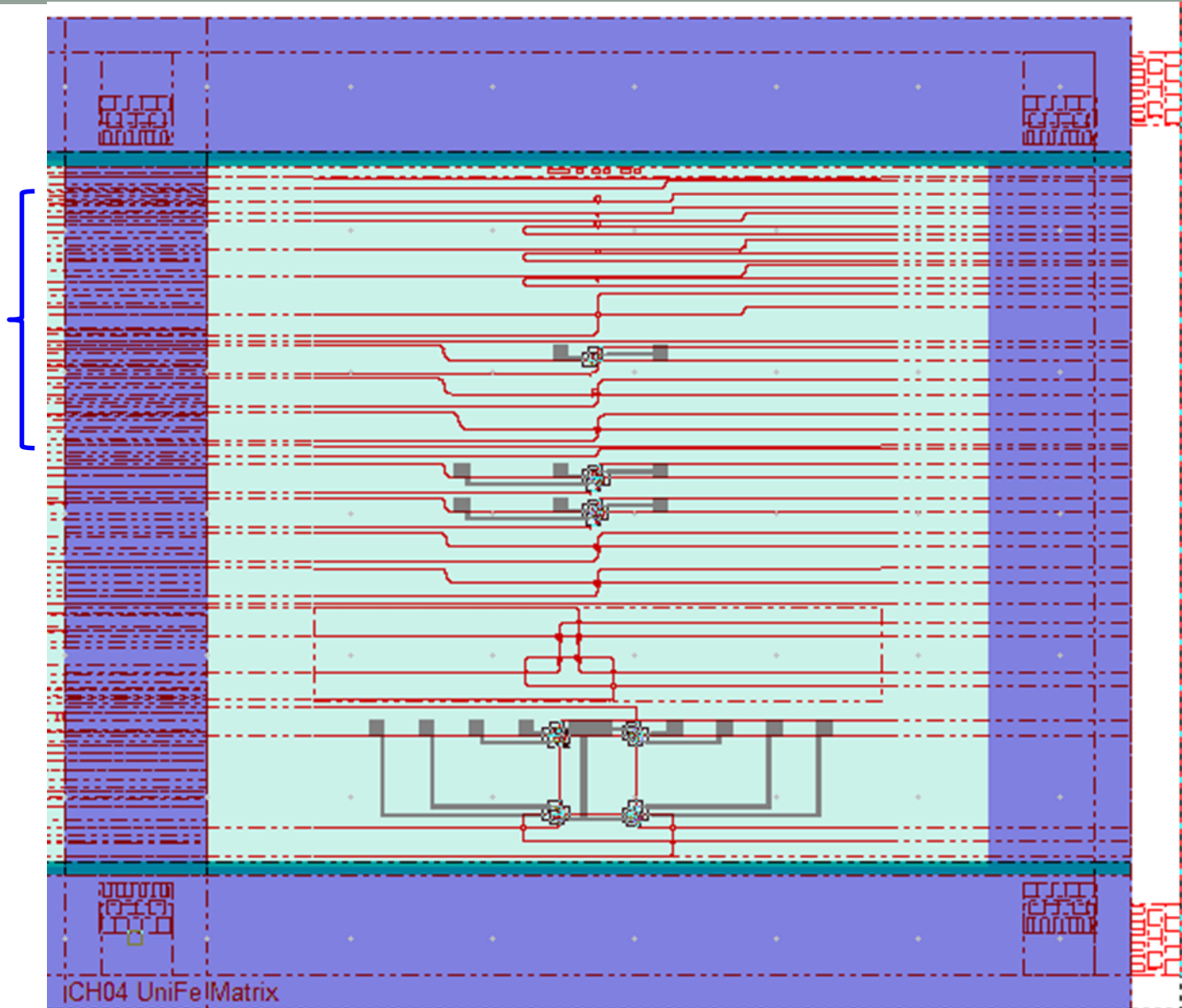




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Waveguides
 1×2 PSE

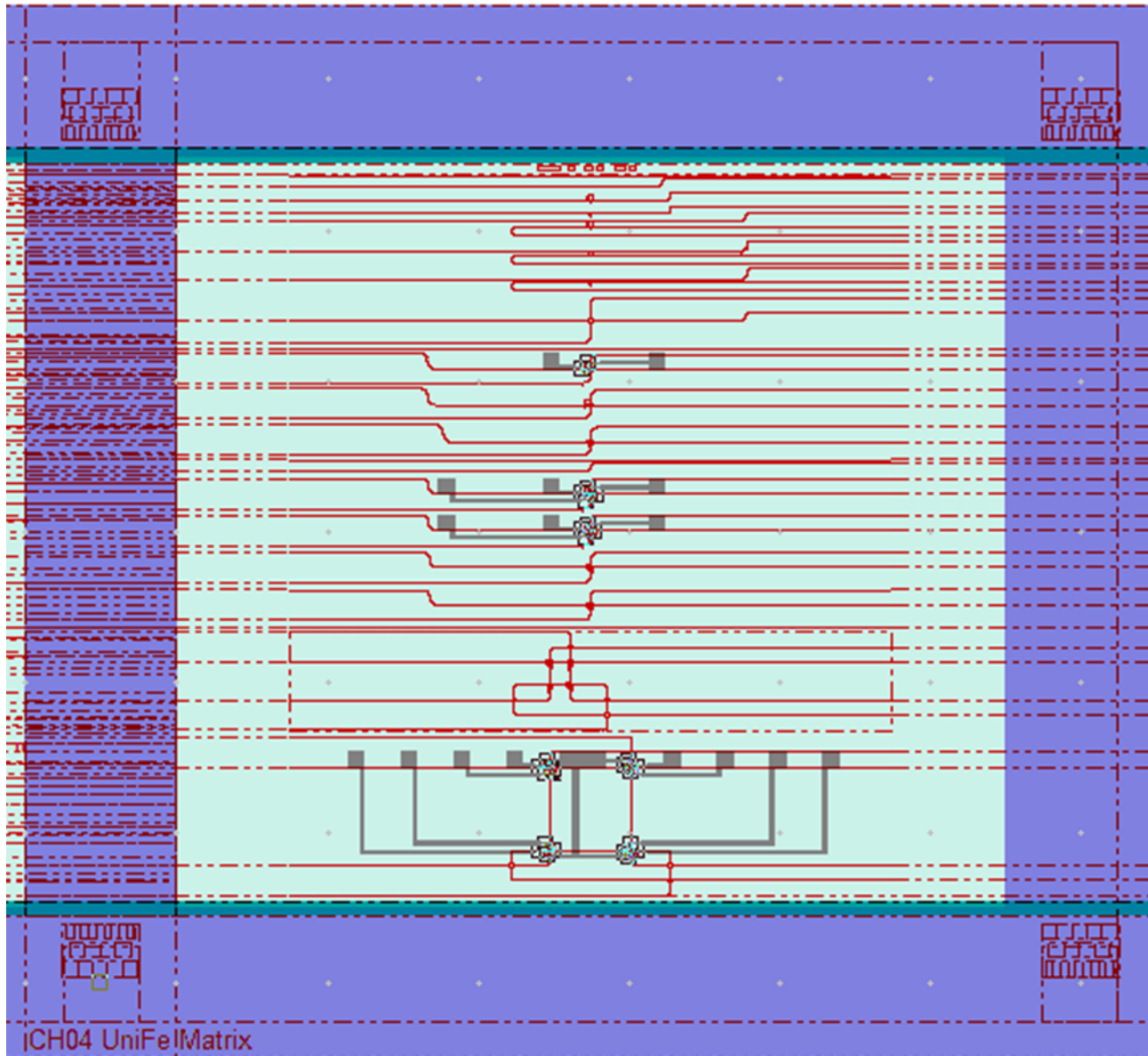


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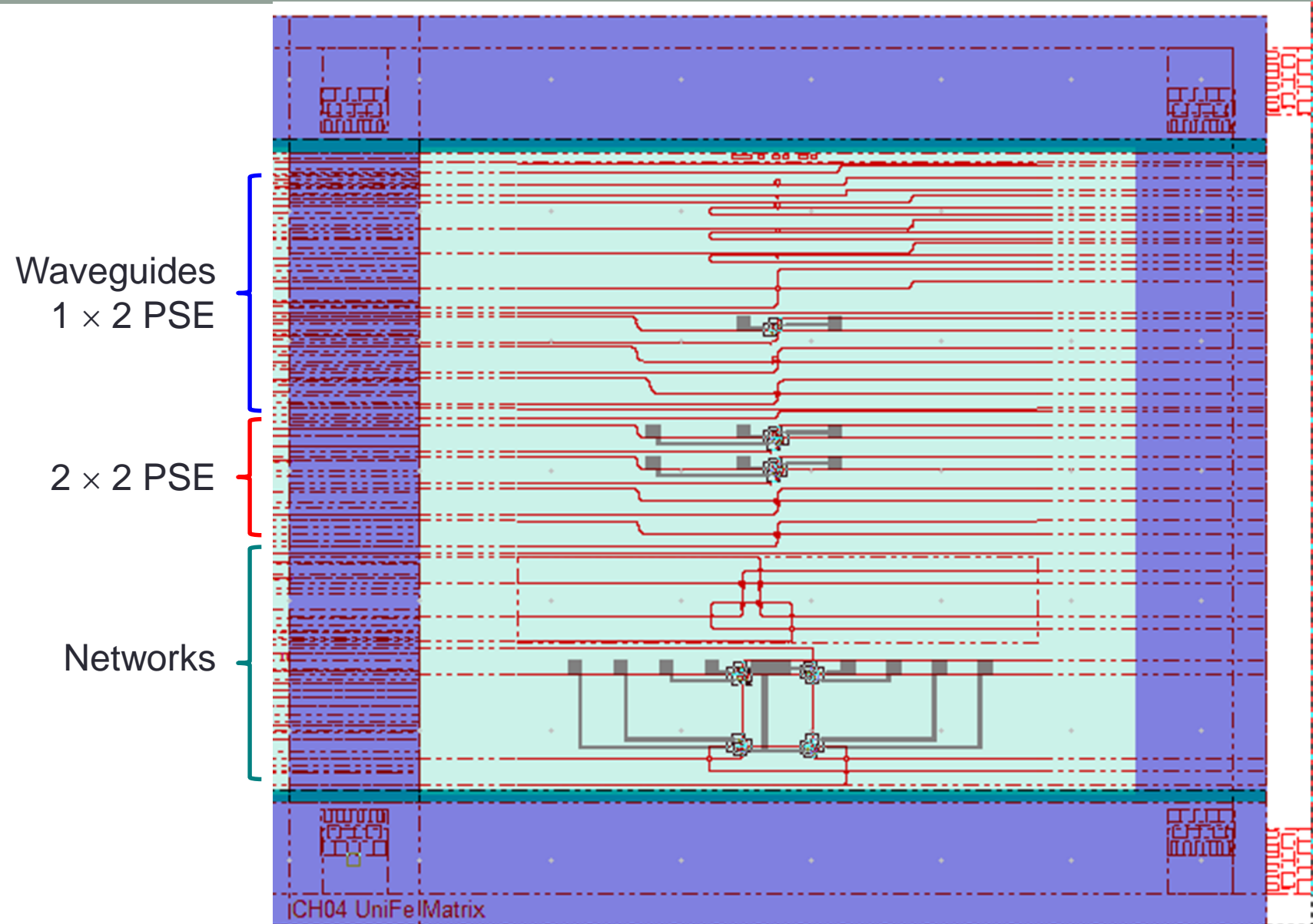
Waveguides
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2×2 PSE



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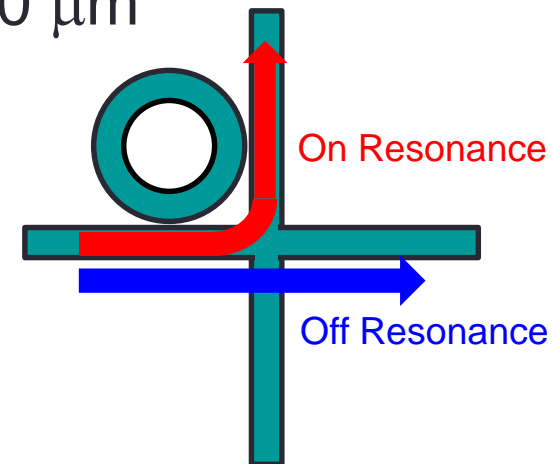
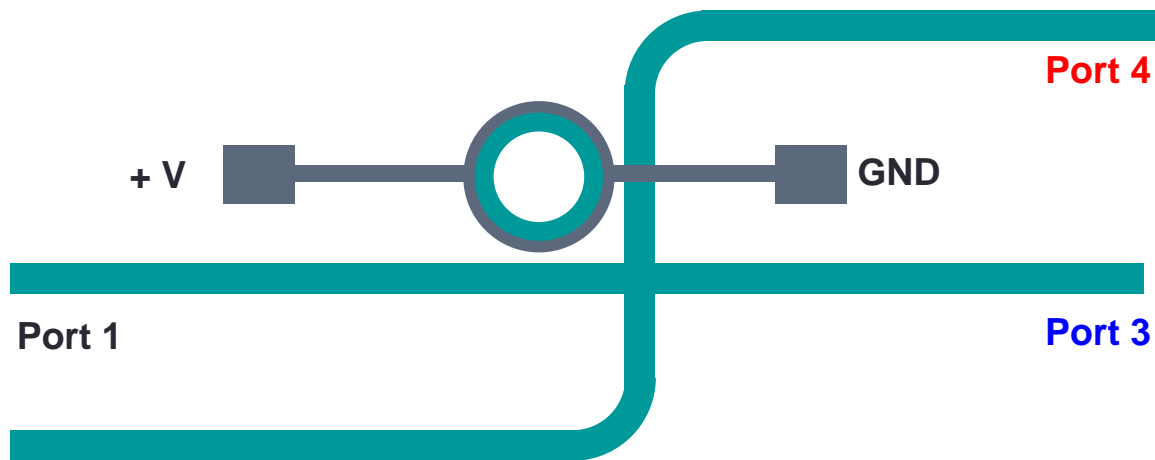




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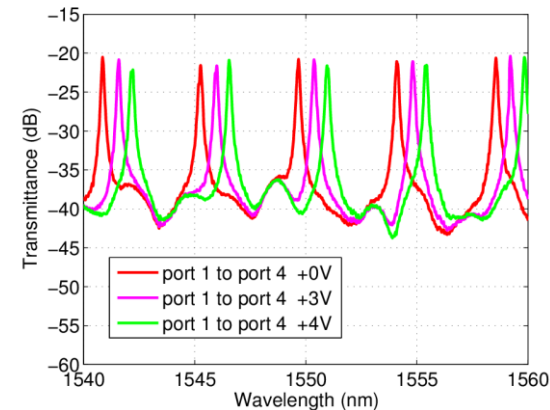
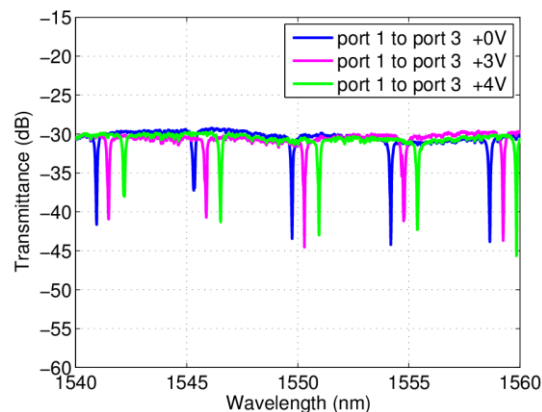
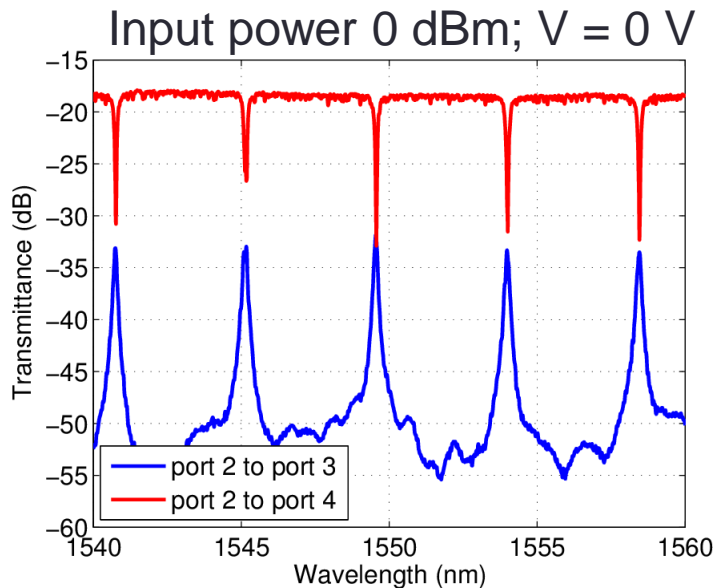


- 1 × 2 Photonic Switching Element - $R = 20 \mu\text{m}$



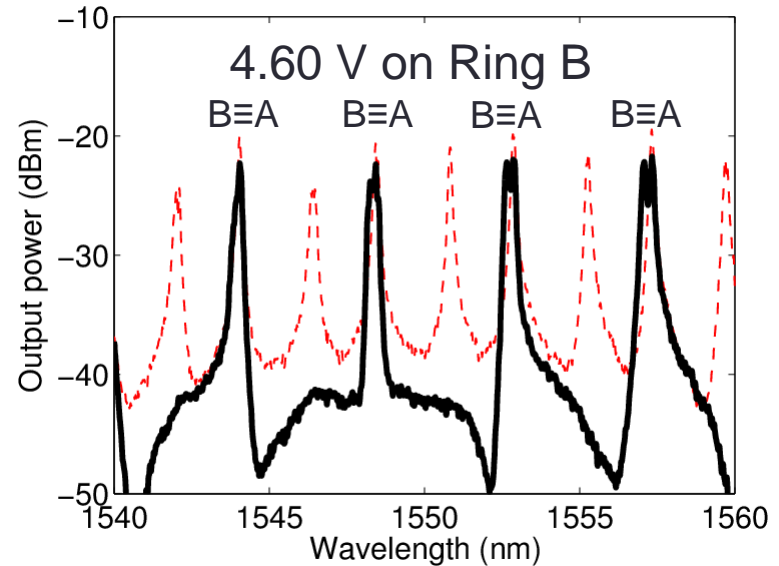
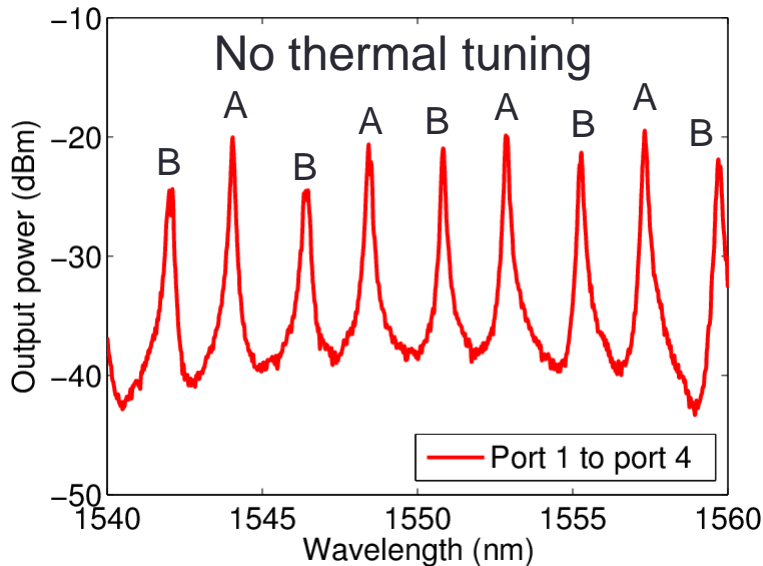
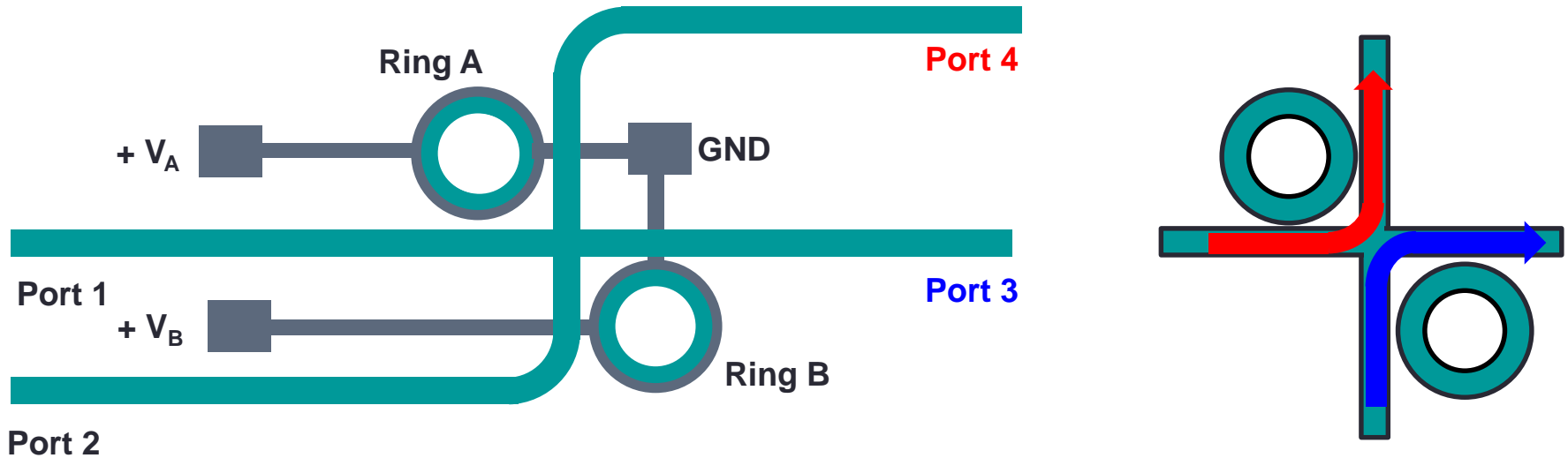
Port 2

Thermal Tuning of the Ring

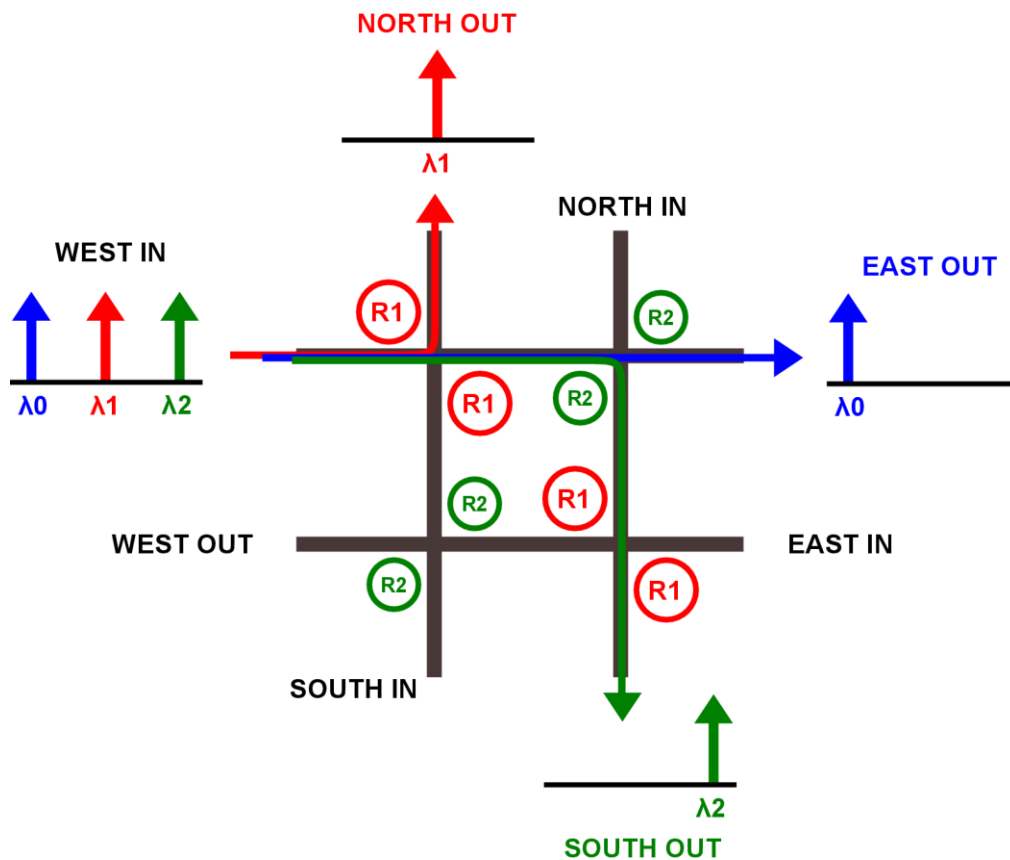


Wavelength shift to power ratio
 0.16 nm/mW (@1550nm)

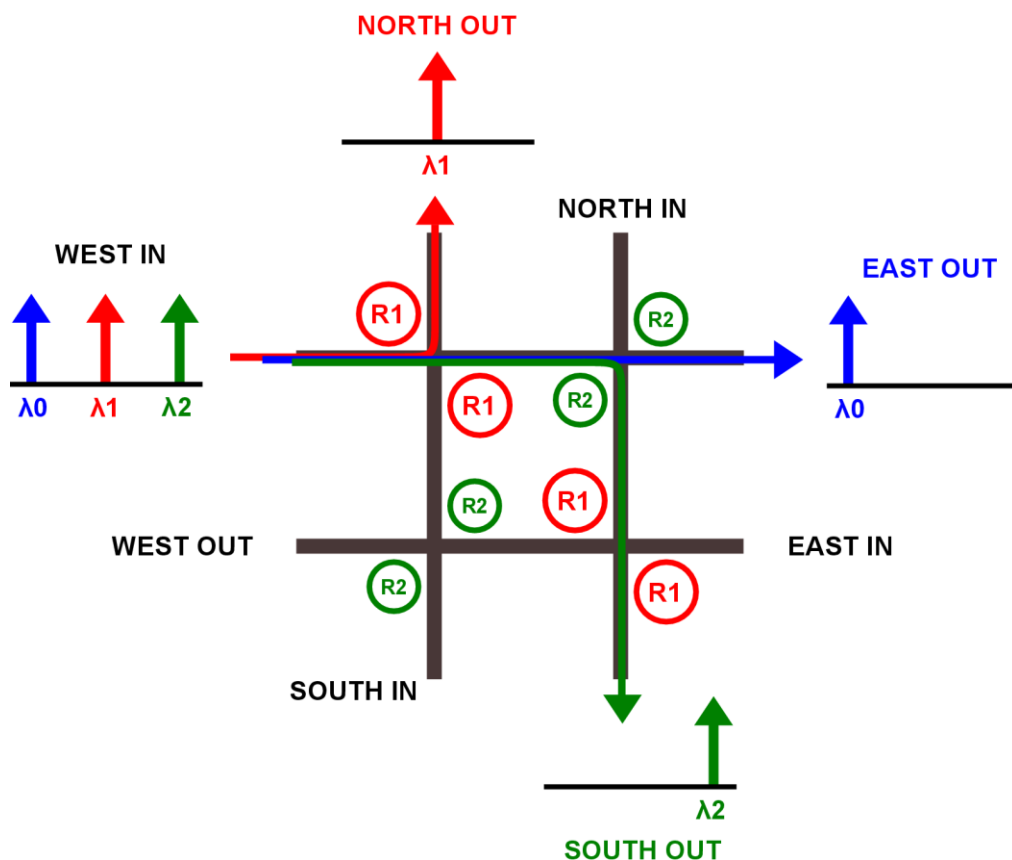
- 2×2 Photonic Switching Element – $R_1 = R_2 = 20 \mu\text{m}$



- Router with 4 Input and 4 output ports GWOR (Generic Wavelength routed Optical Router)



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- Wavelength dependent routing achieved through the choice of different radii for rings **R1** and **R2**

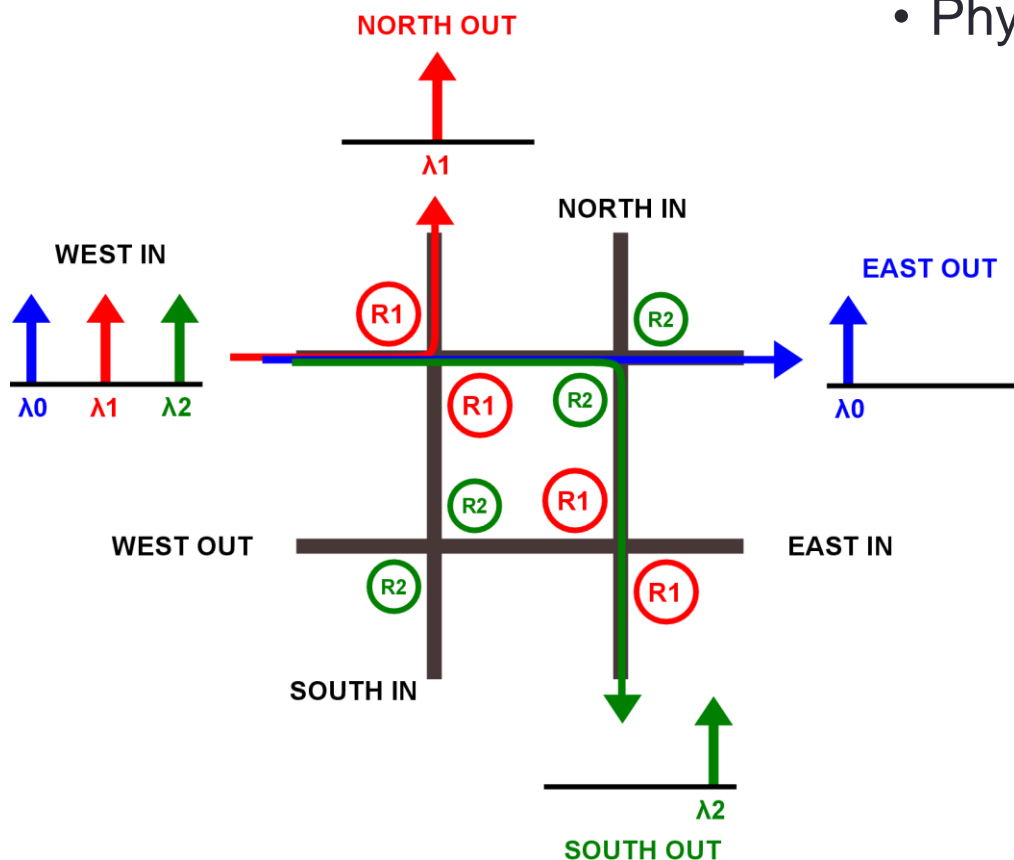


Routing Table

	NORTH OUT	EAST OUT	SOUTH OUT	WEST OUT
NORTH IN	-	λ_2		λ_1
EAST IN	λ_2	-	λ_1	
SOUTH IN	λ_0	λ_1	-	λ_2
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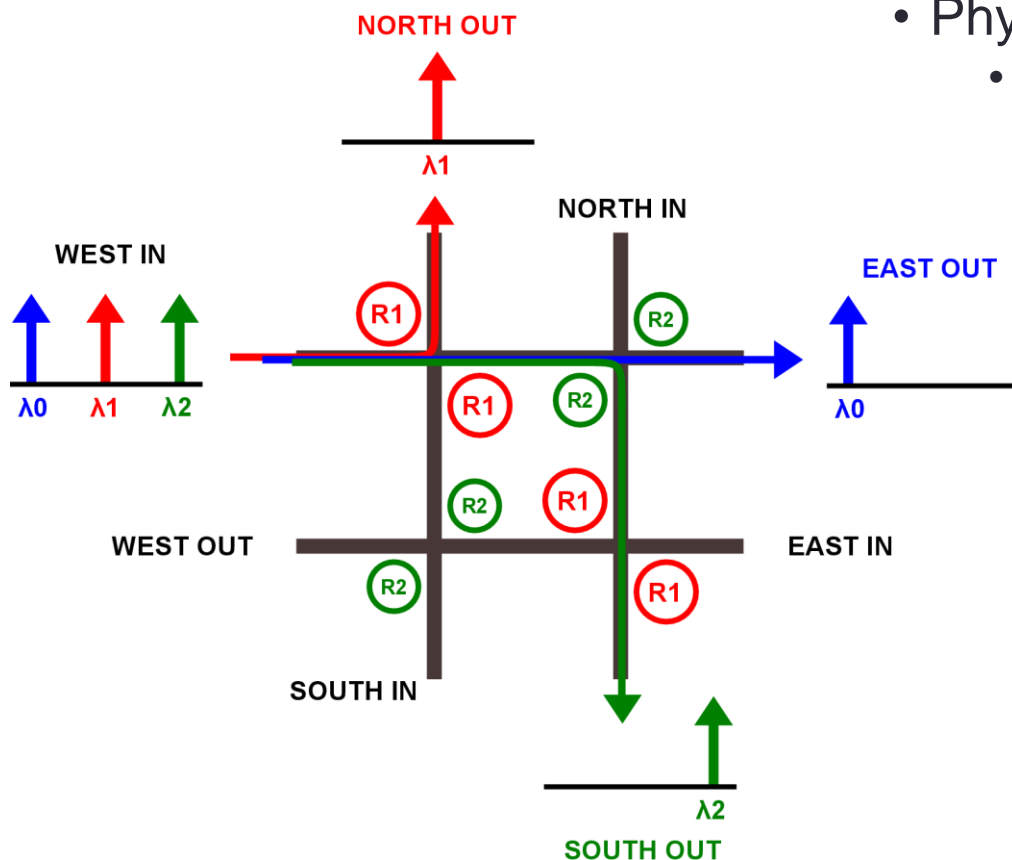
- Physical Parameters



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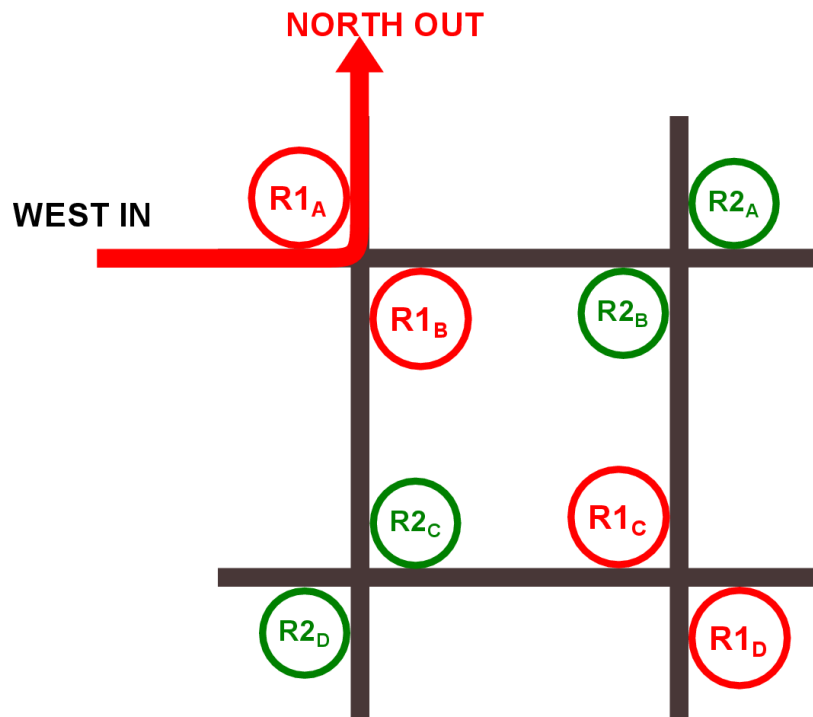
Physical Parameters

- Bus-to-ring gap 150 nm (power coupling $K = 7.5\%$)
- **R1 = 20 μm Bandwidth = 15.5 GHz**
- **R2 = 18 μm Bandwidth = 17.5 GHz**

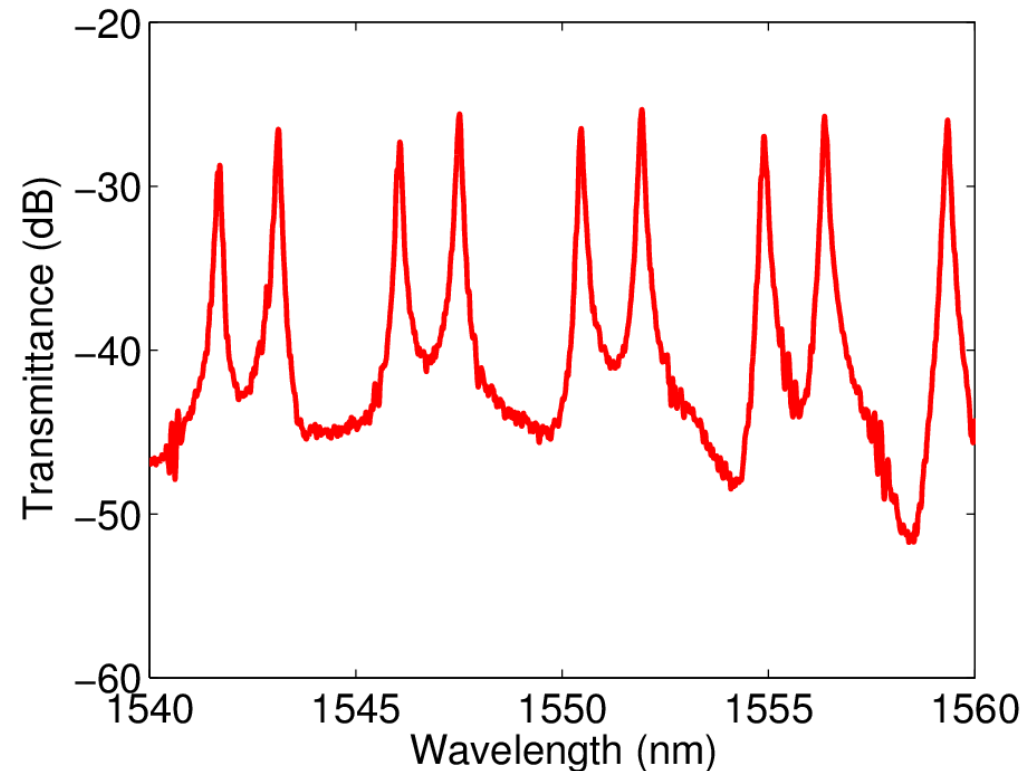
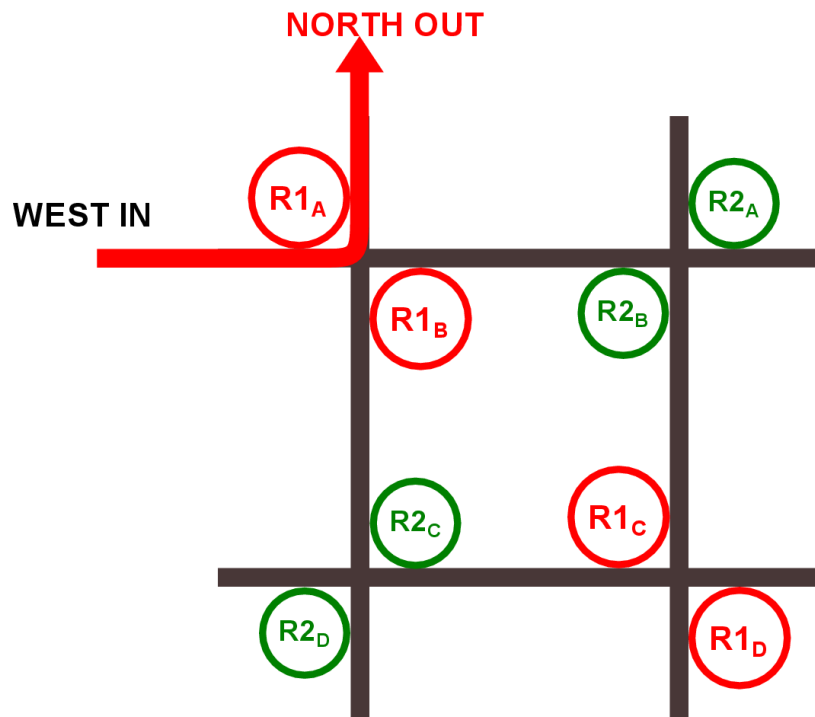
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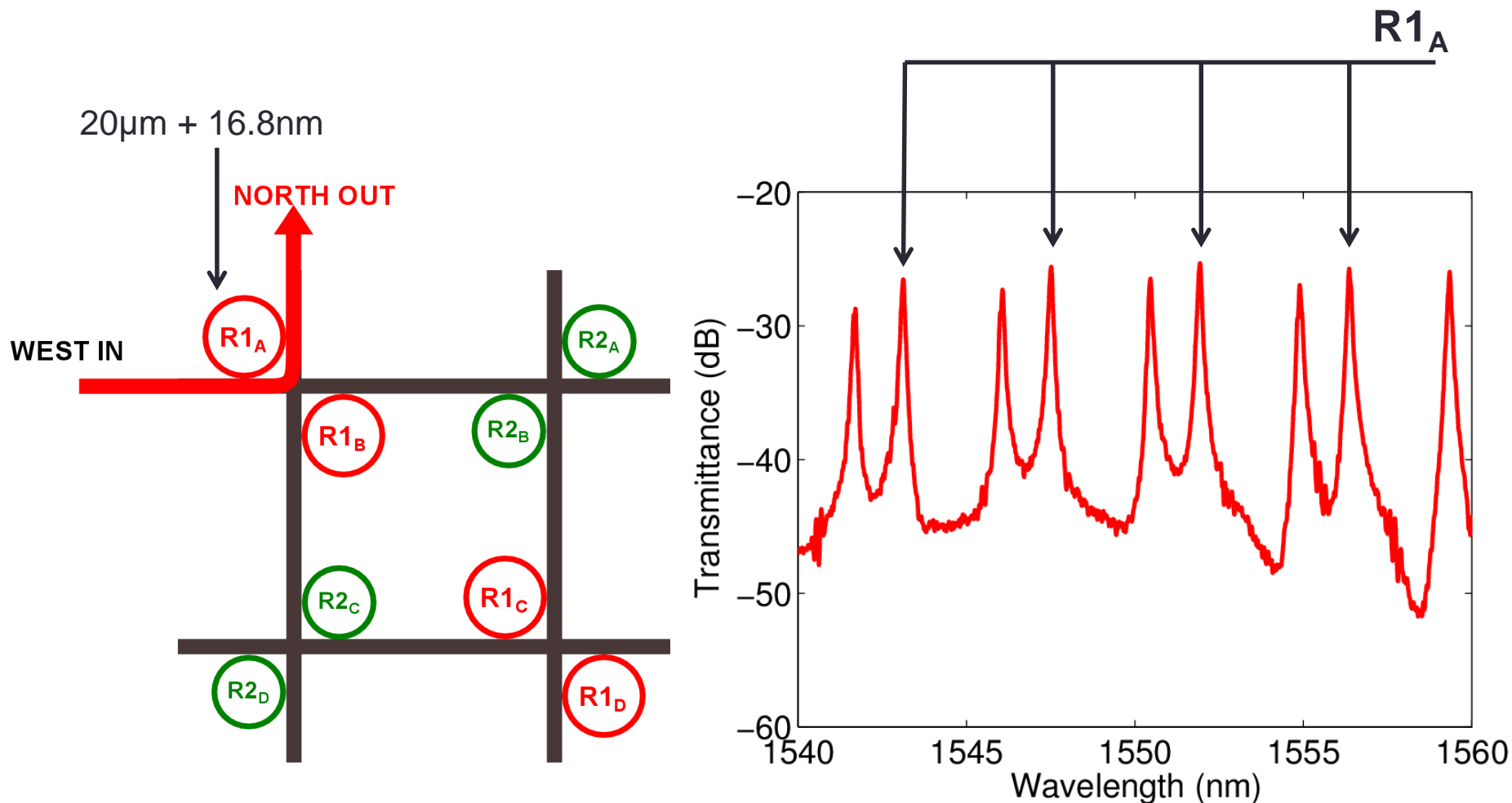
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 - Misalignment in the radii of $R1_A$ and $R1_B$ with respect to the design value ($20\ \mu\text{m}$)



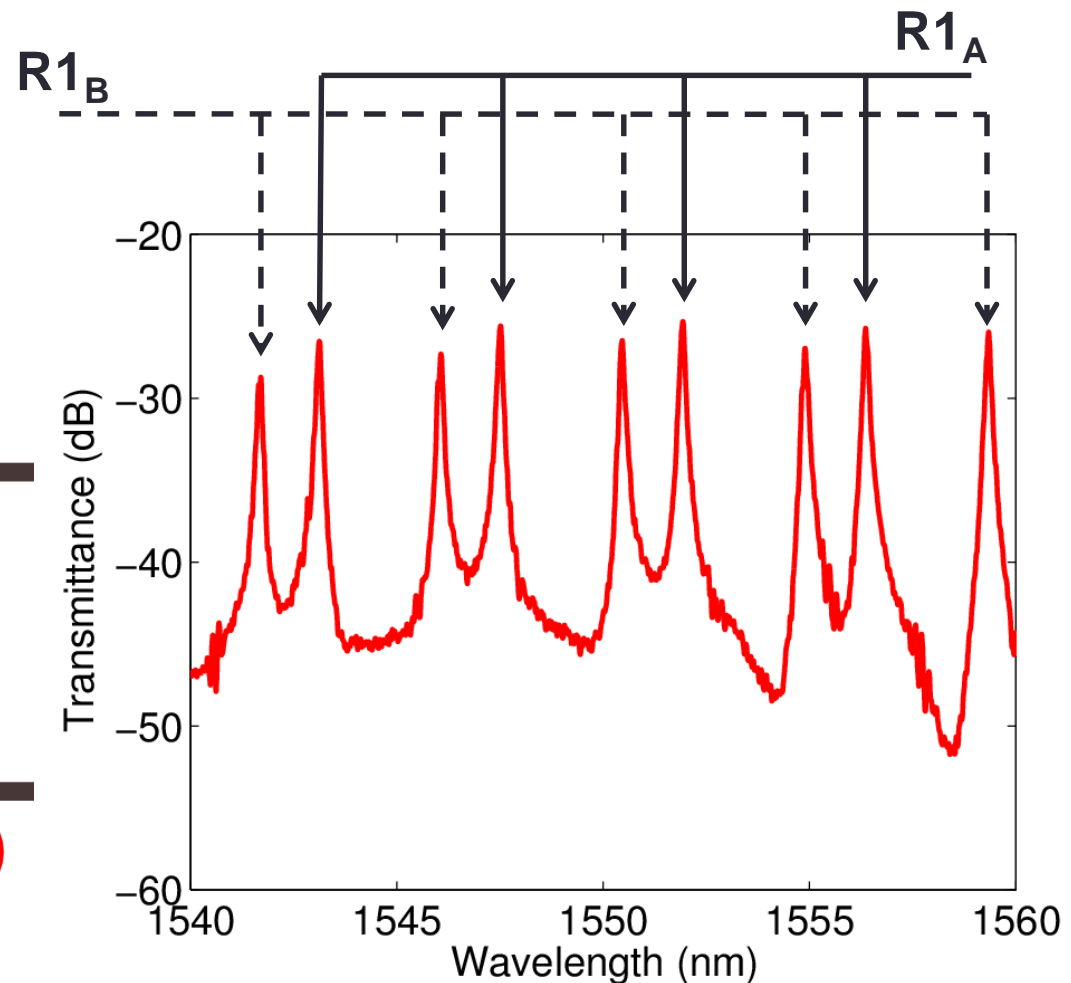
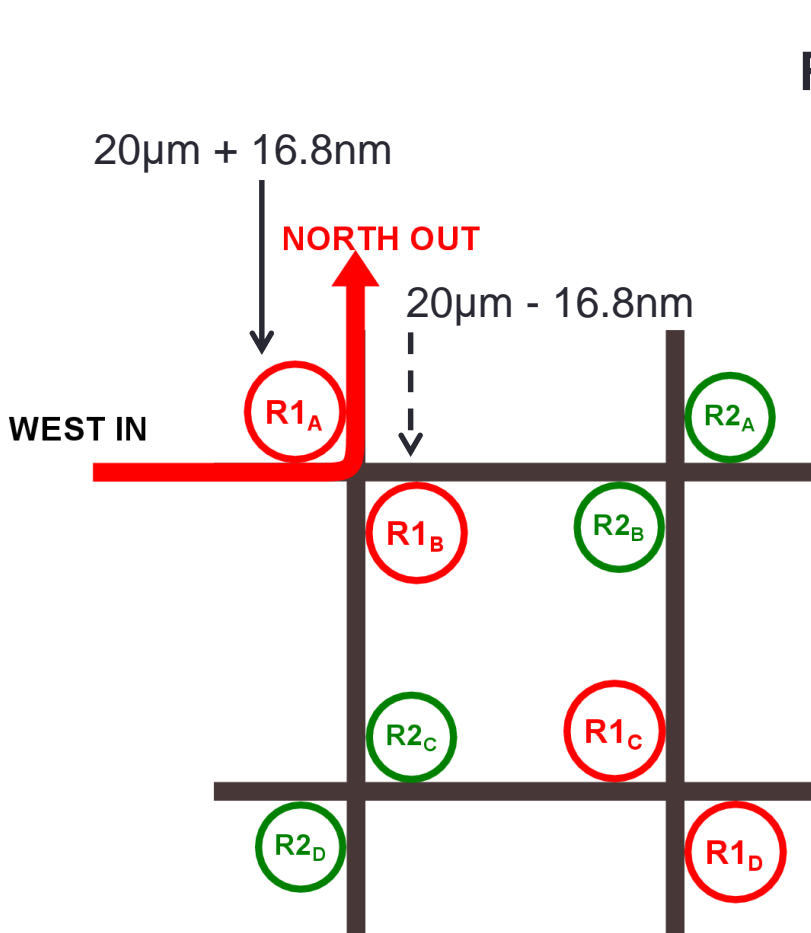
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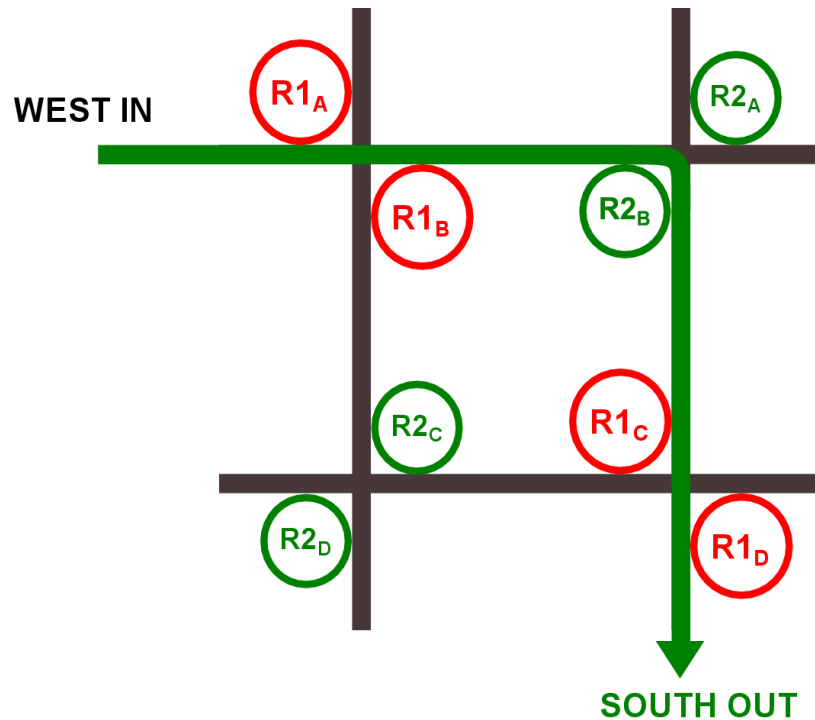
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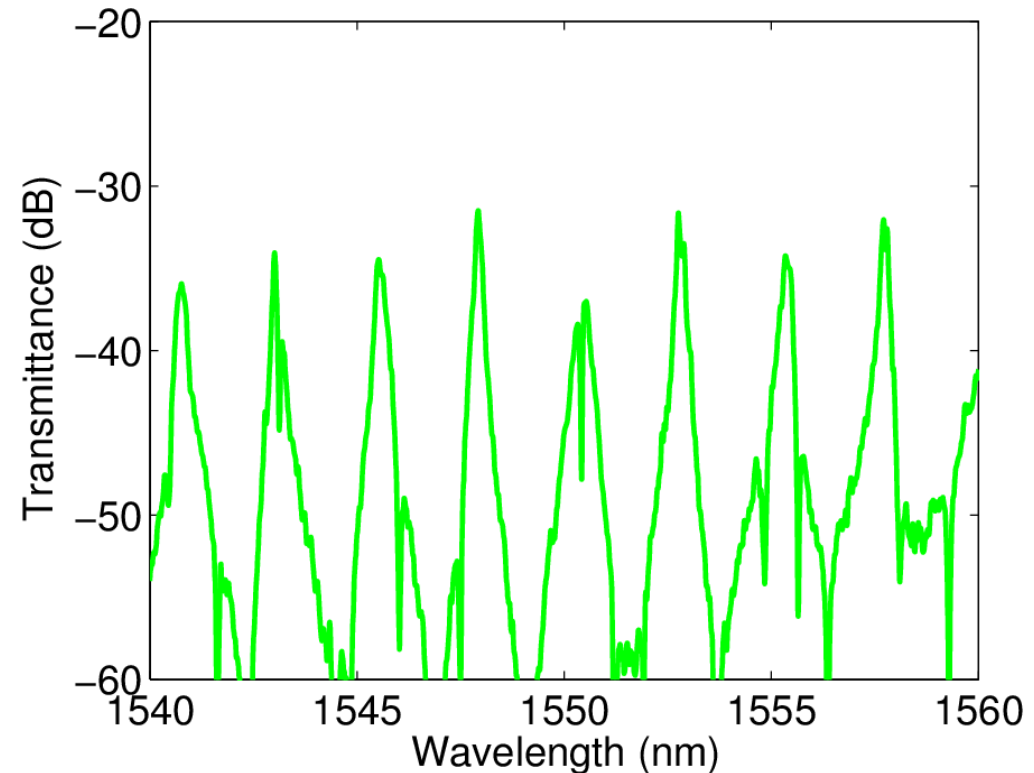
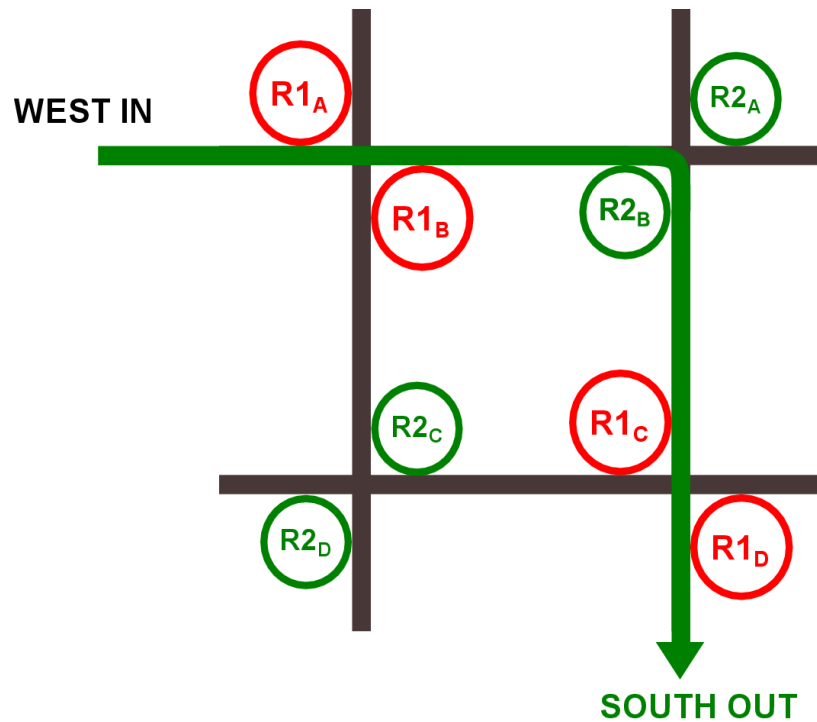
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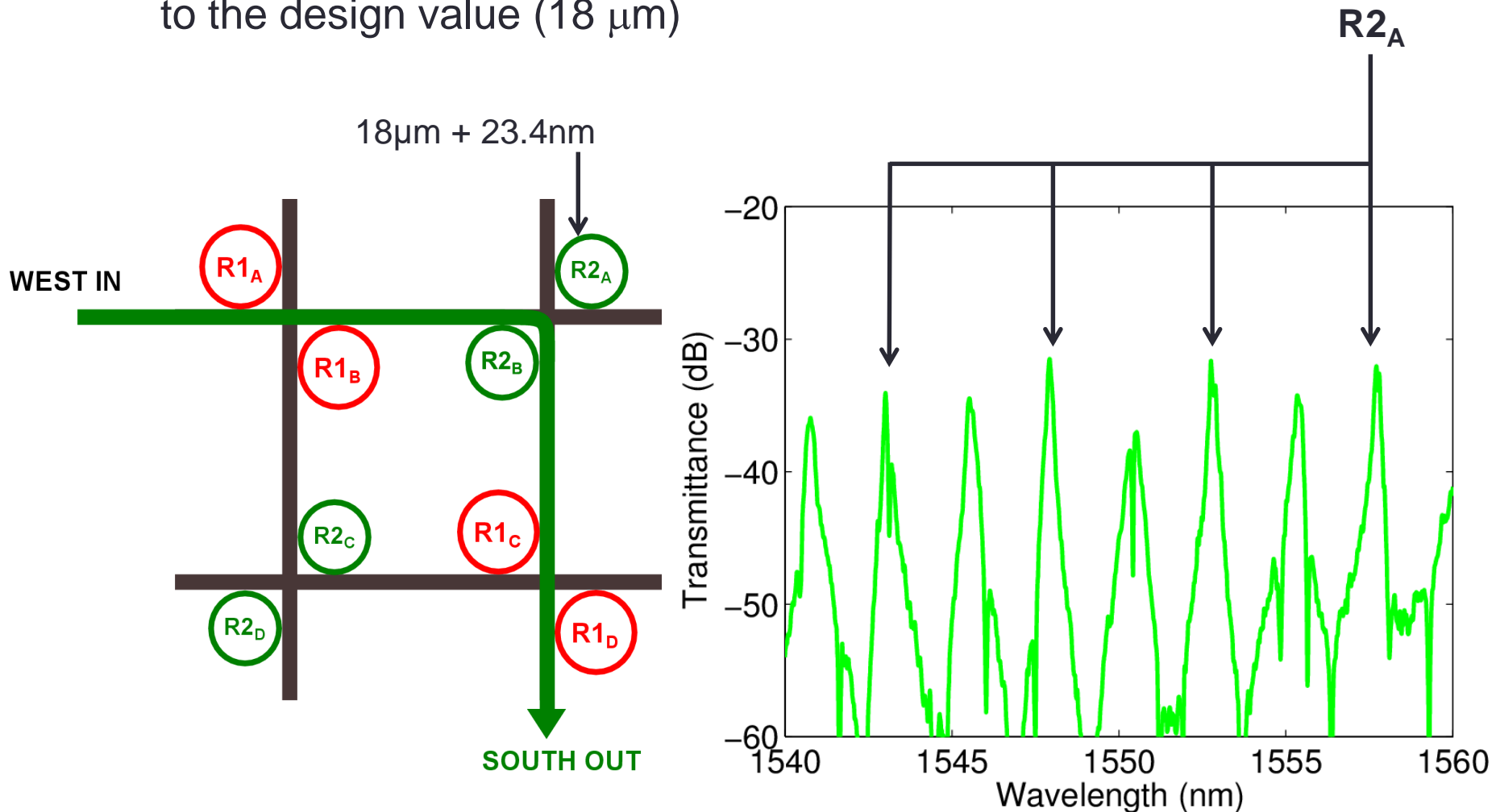
- Resonance Duplication due to the fabrication process
 - Misalignment in the radii of $R2_A$ and $R2_B$ with respect to the design value ($18\ \mu\text{m}$)



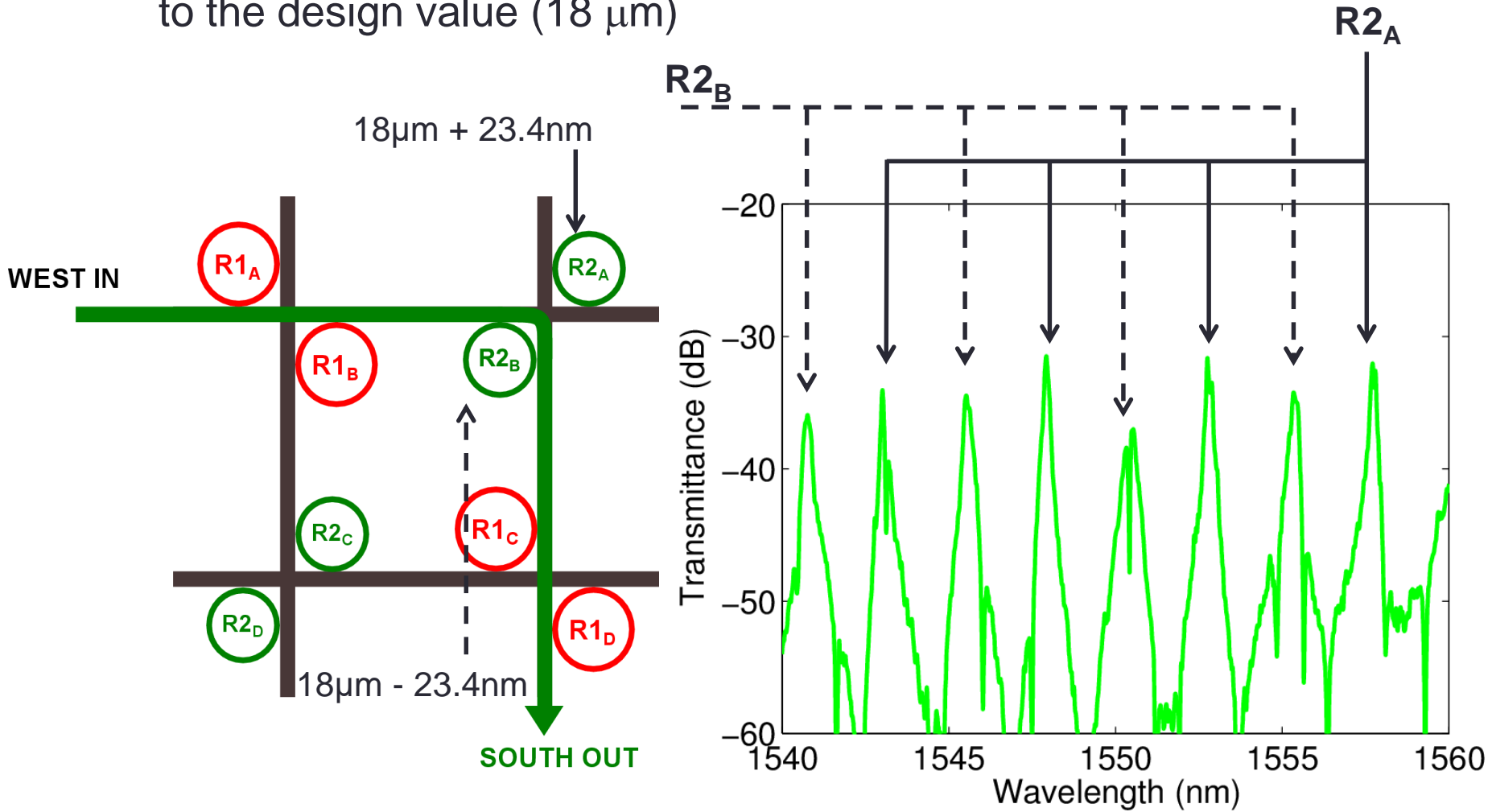
- Resonance Duplication due to the fabrication process
 - Misalignment in the radii of $R2_A$ and $R2_B$ with respect to the design value ($18\ \mu\text{m}$)



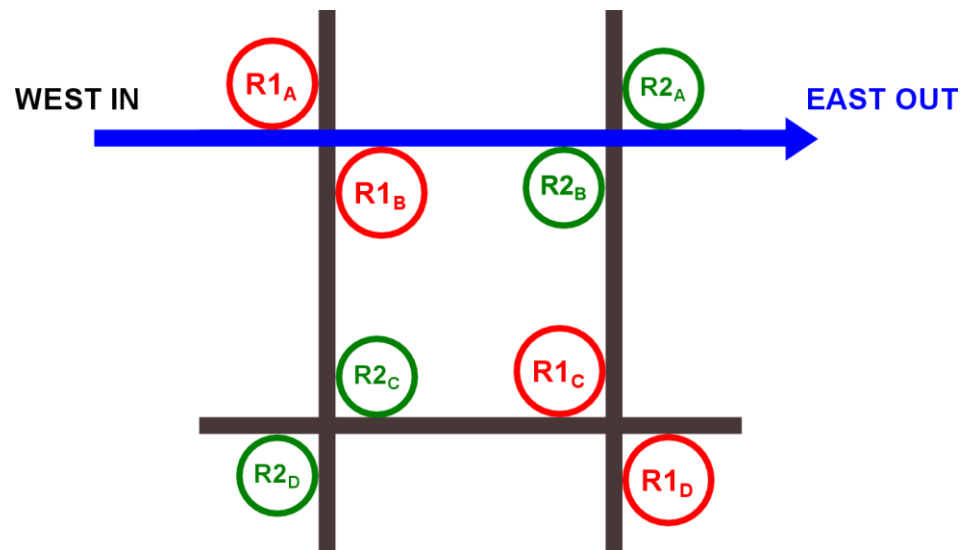
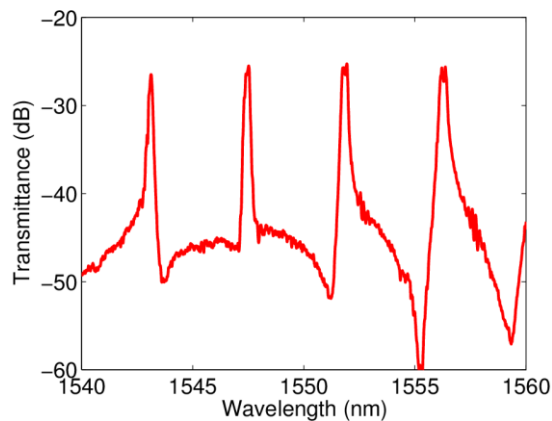
- Resonance Duplication due to the fabrication process
 - Misalignment in the radii of $R2_A$ and $R2_B$ with respect to the design value ($18\ \mu\text{m}$)



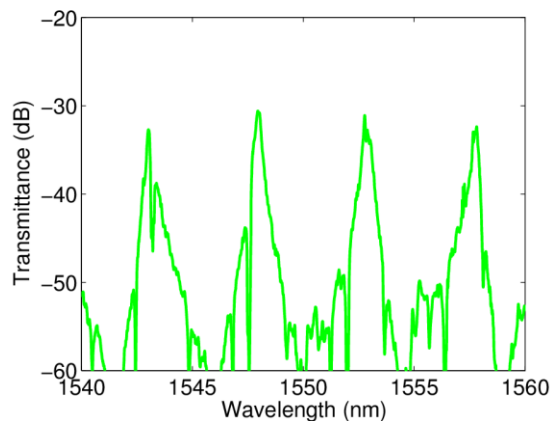
- Resonance Duplication due to the fabrication process
 - Misalignment in the radii of $R2_A$ and $R2_B$ with respect to the design value ($18\ \mu\text{m}$)



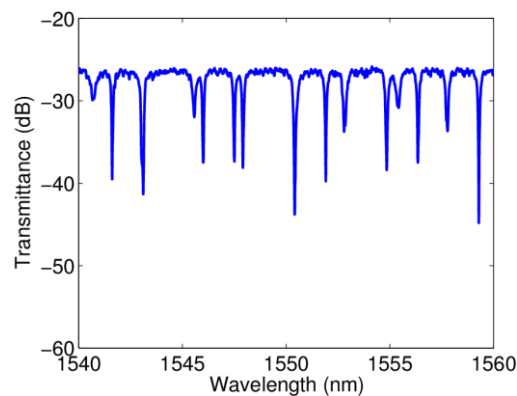
Tuning by applying 4.42 V on R1_B



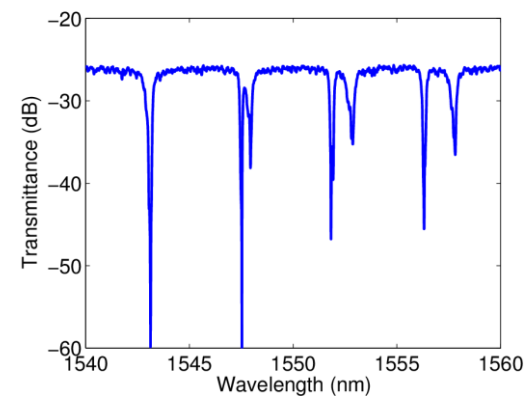
Tuning by applying 4.62 V on R2_B



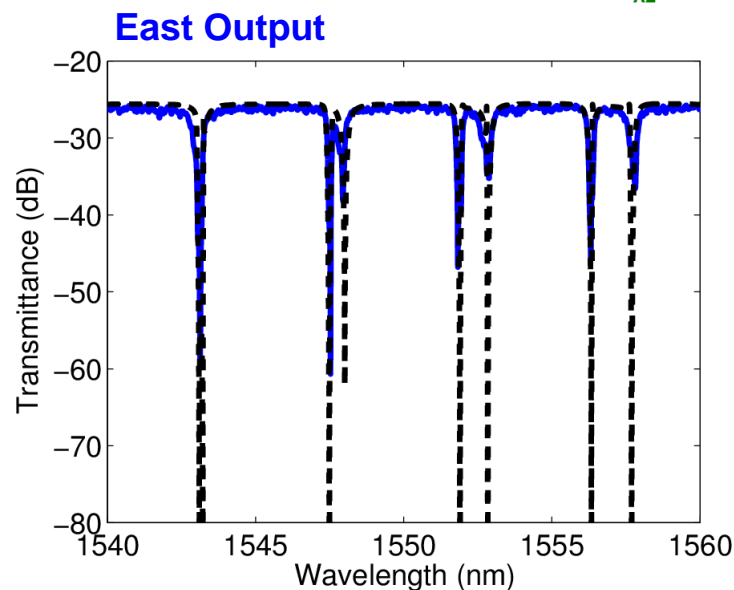
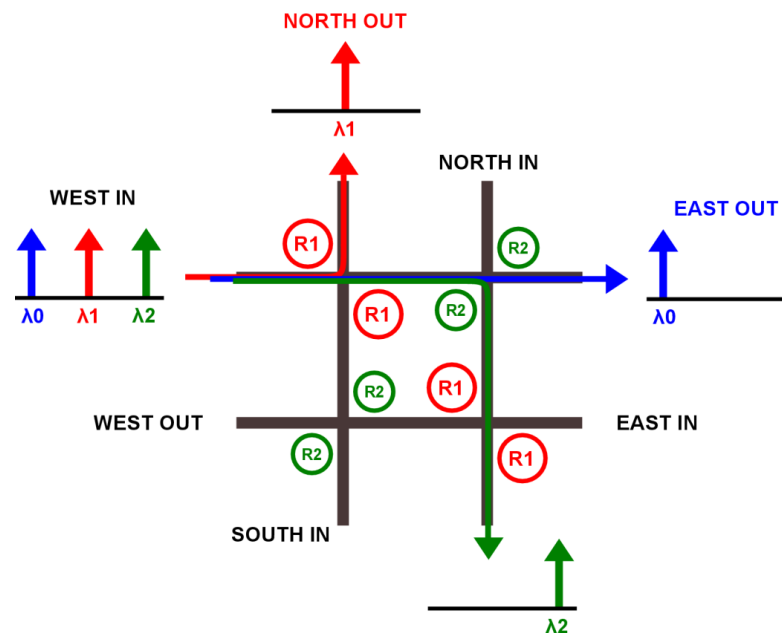
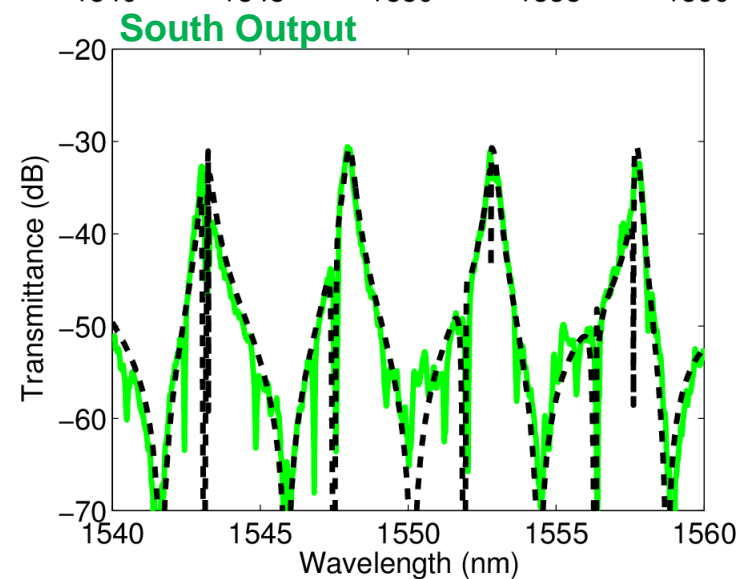
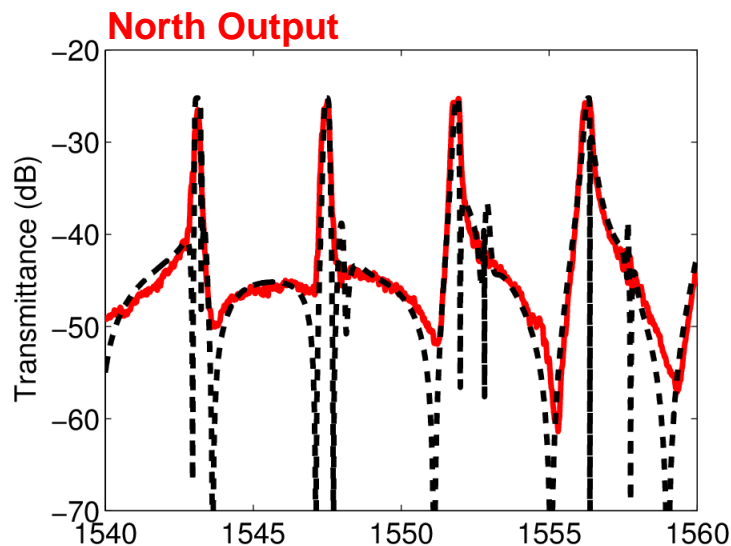
Tuning Off



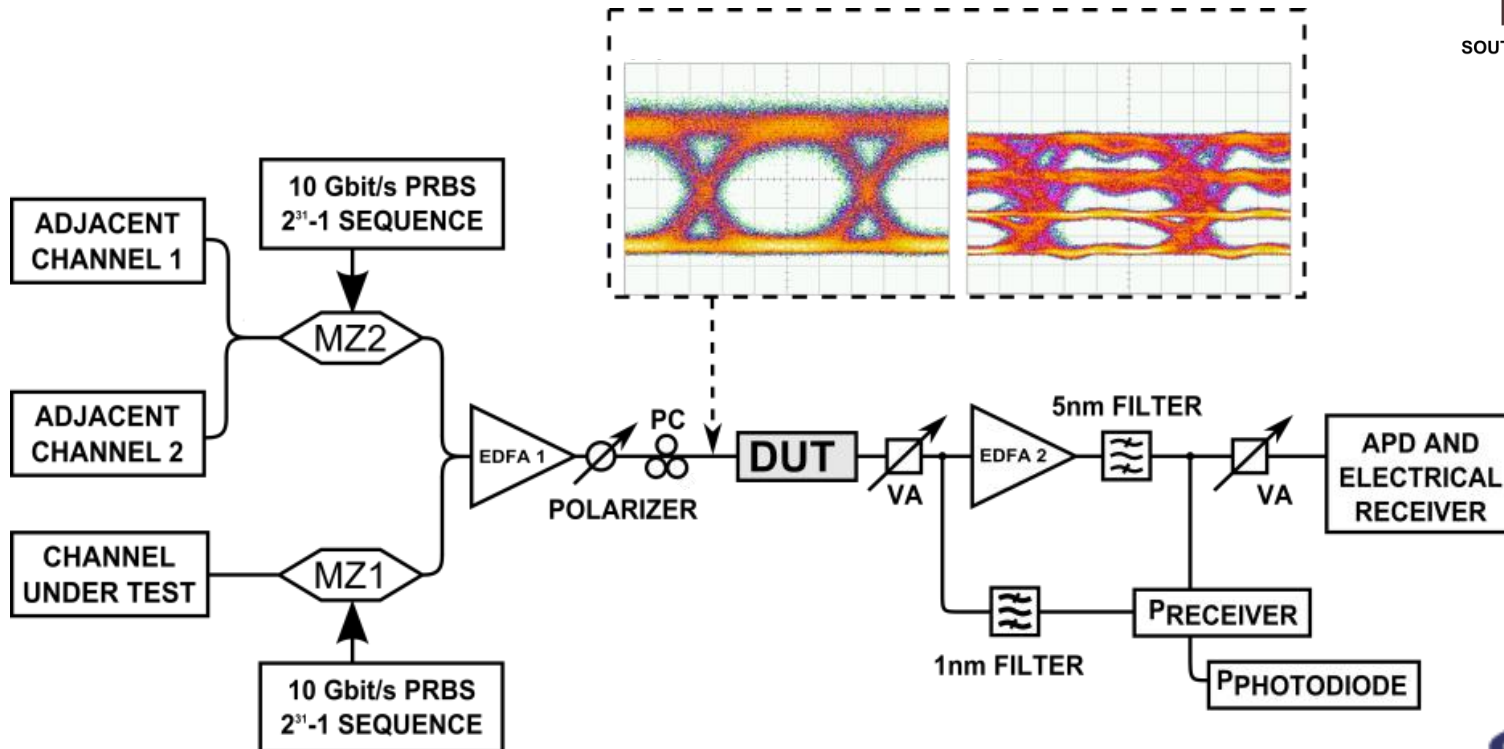
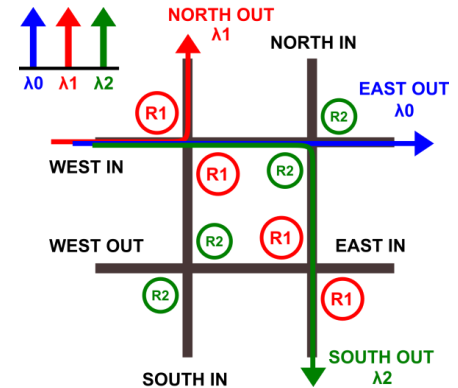
Tuning On

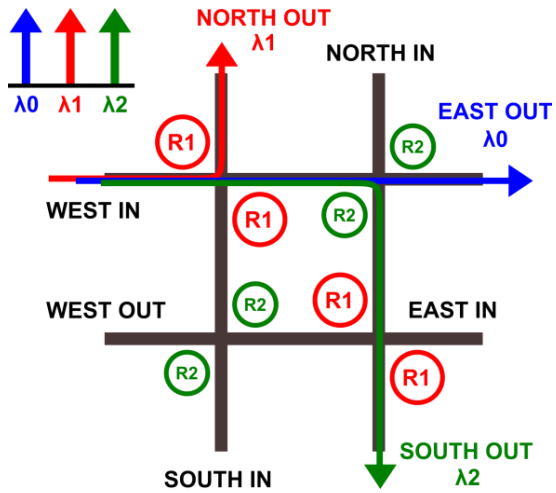


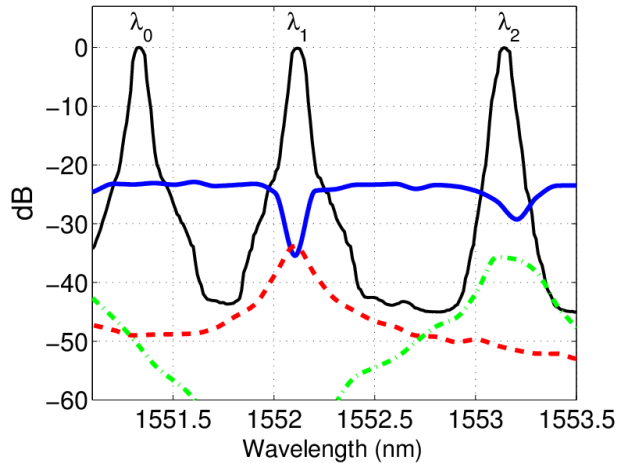
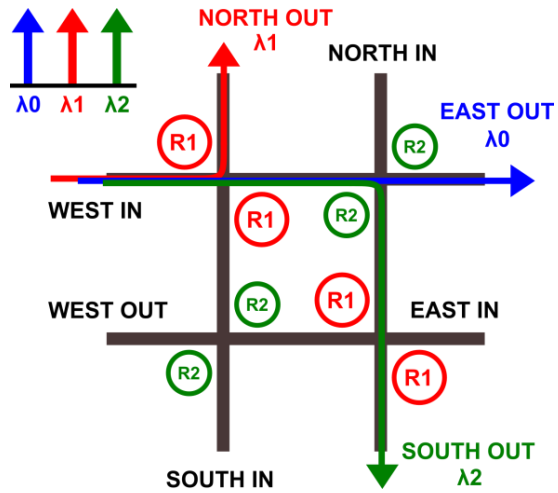
S-Matrix vs Measurements

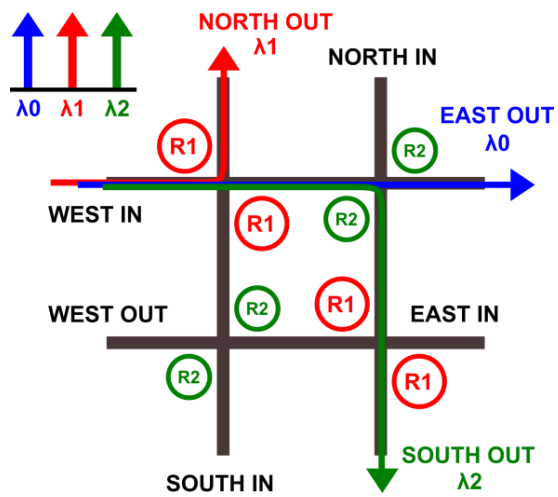


- BER Evaluation - Two dual configurations:
 - Single channel (10 Gbit/s)
 - 3-channels (3×10 Gbit/s) WDM

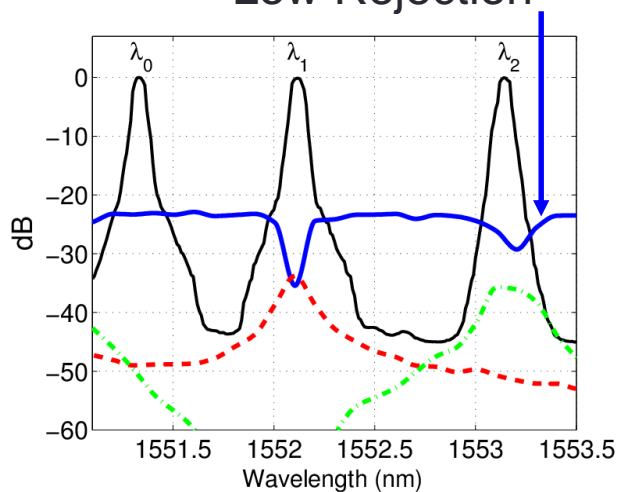


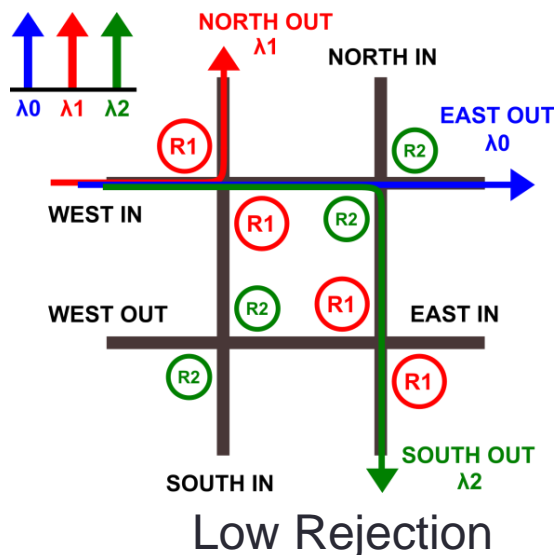




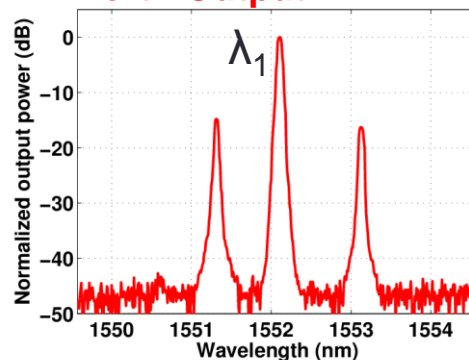


Low Rejection

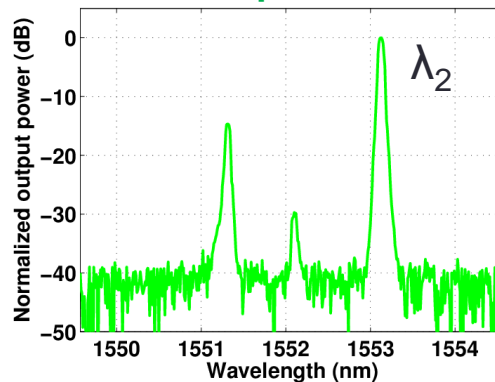




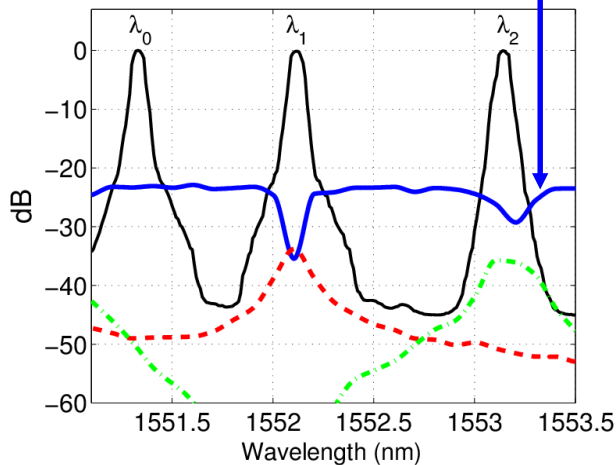
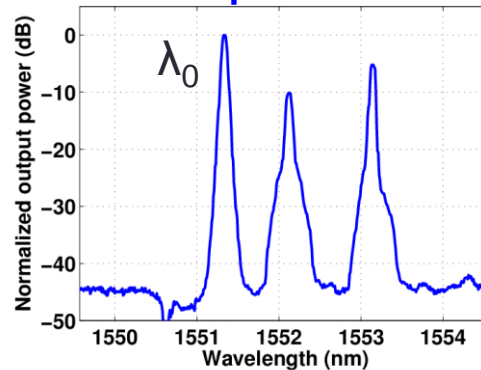
North Output

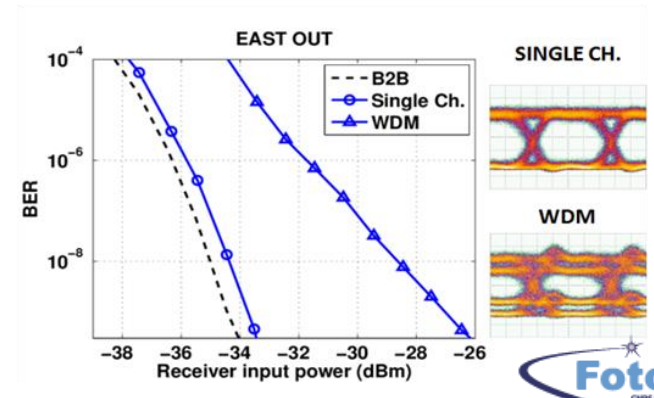
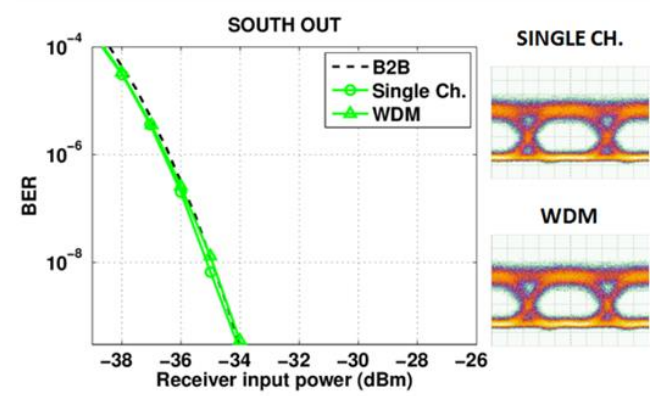
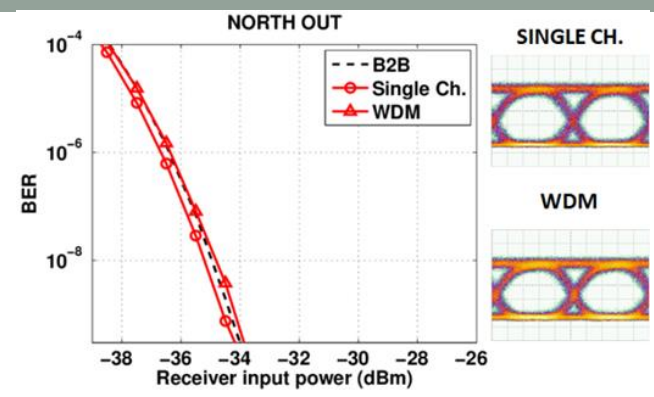
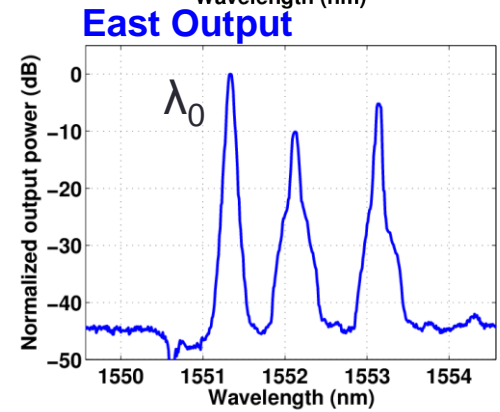
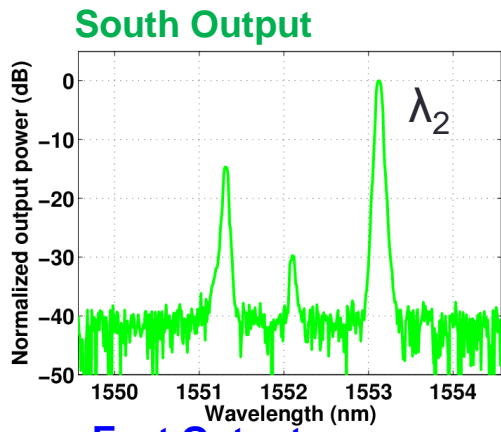
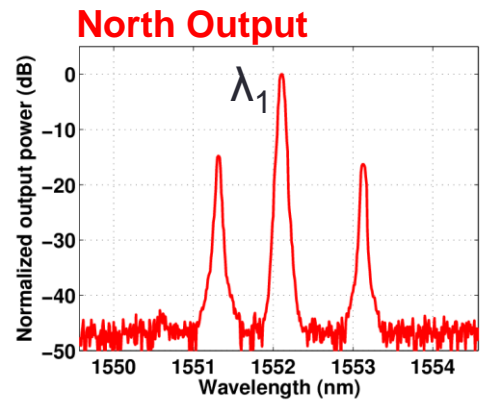
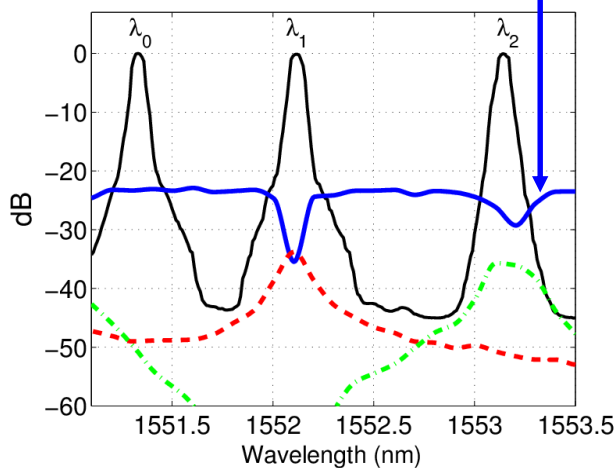
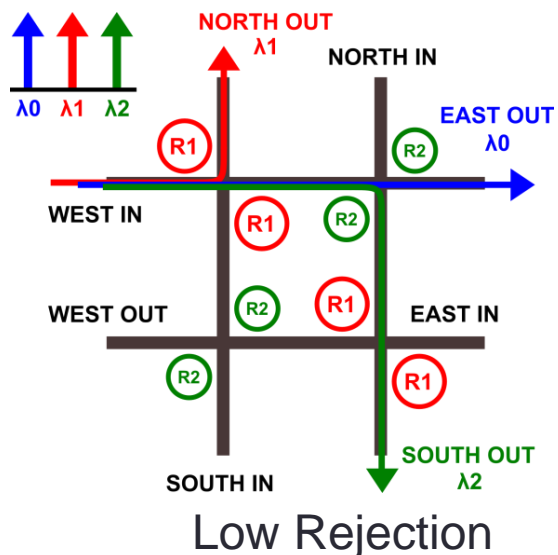


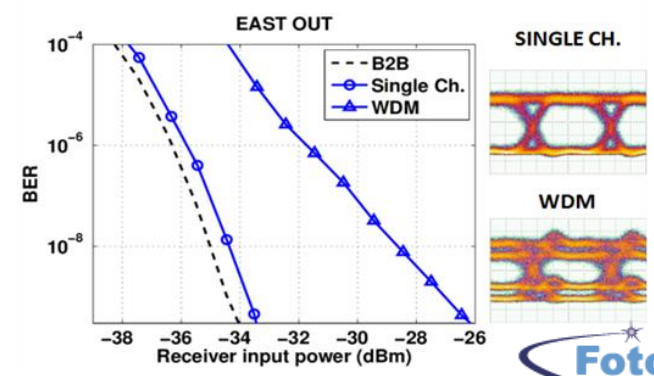
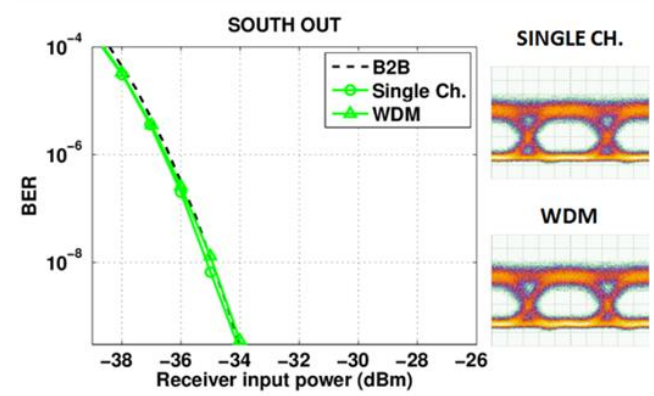
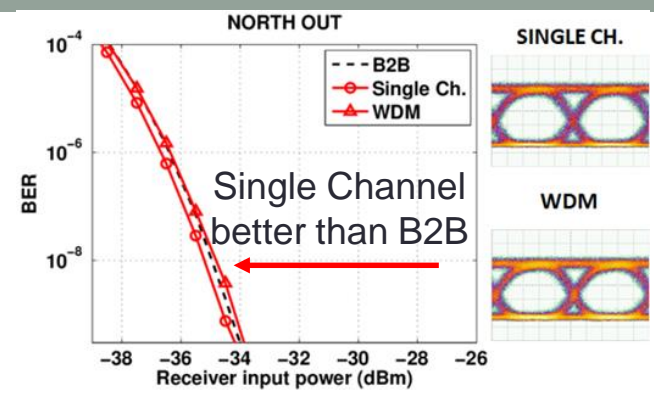
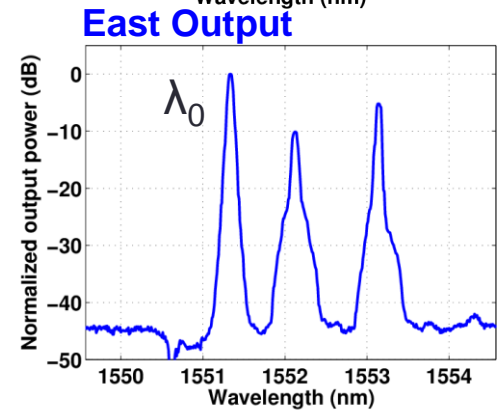
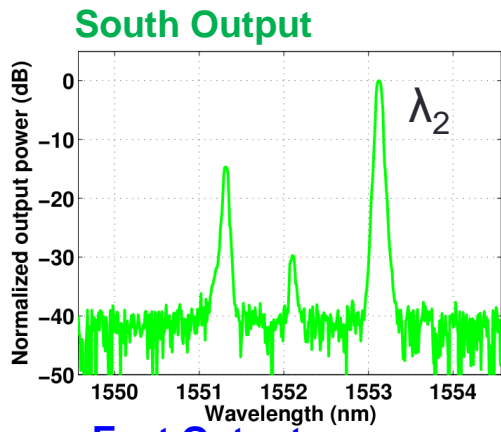
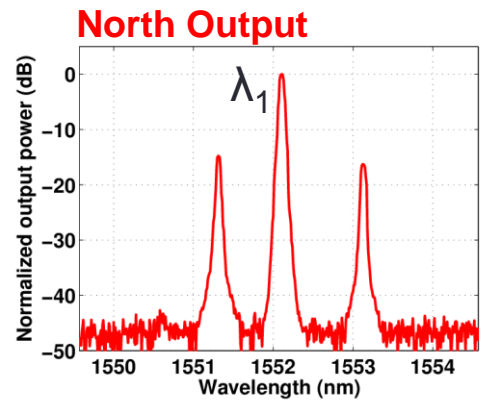
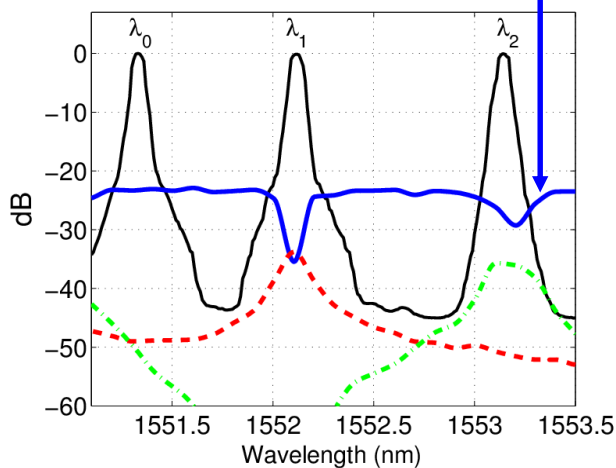
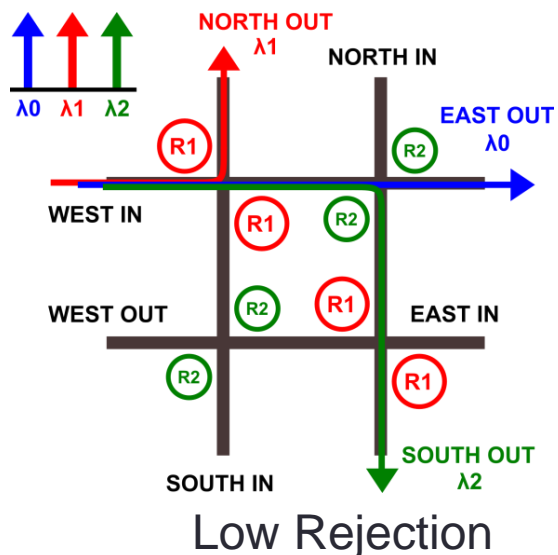
South Output

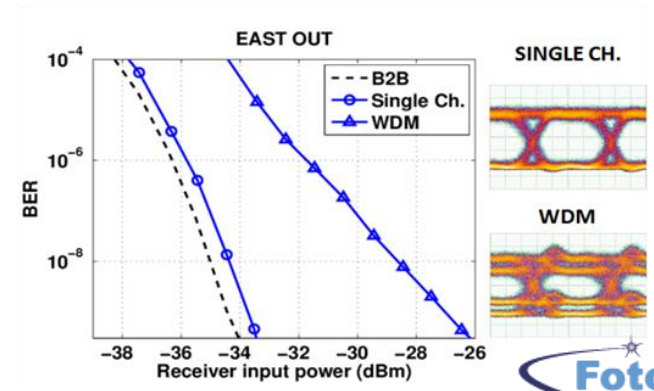
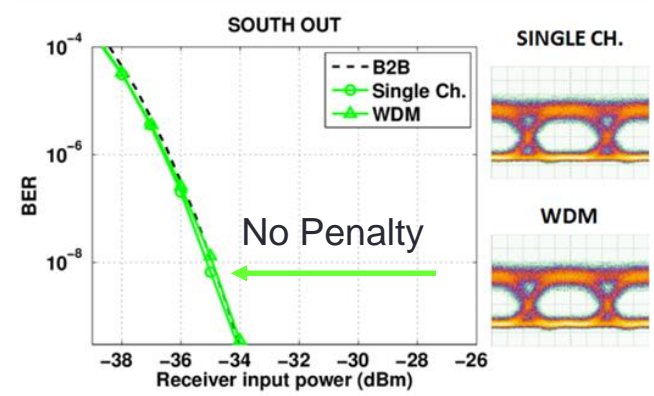
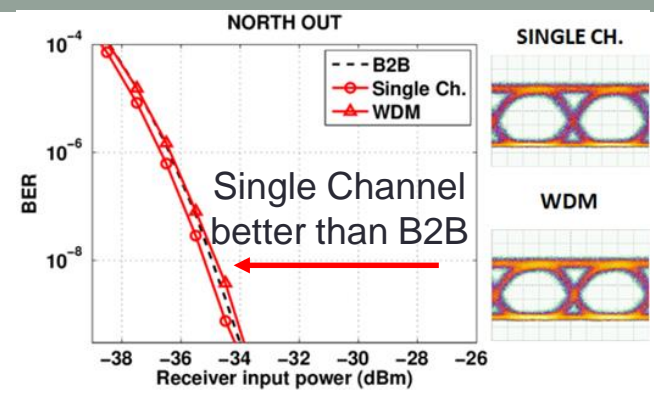
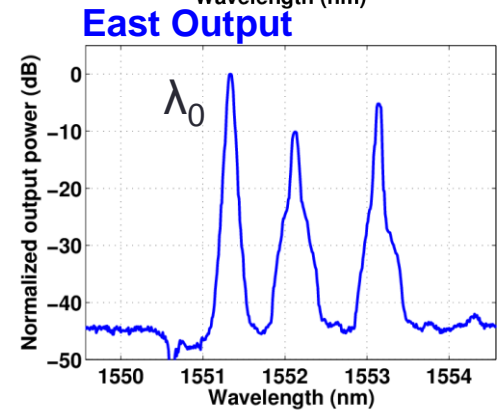
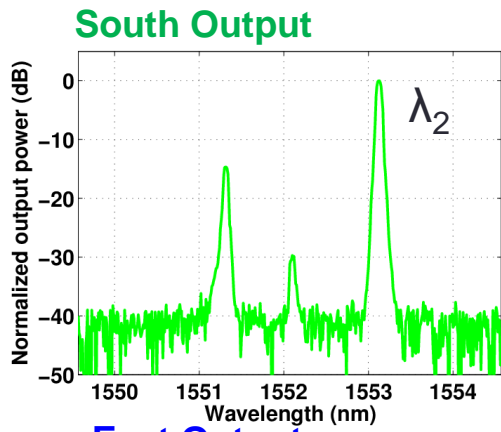
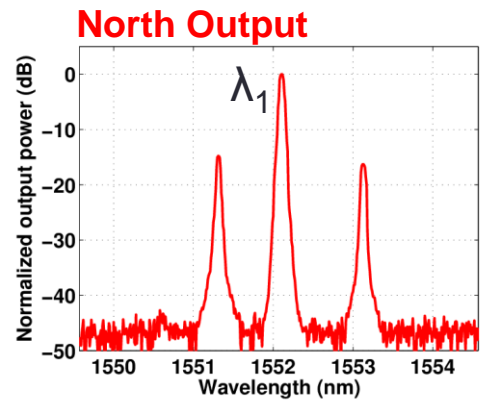
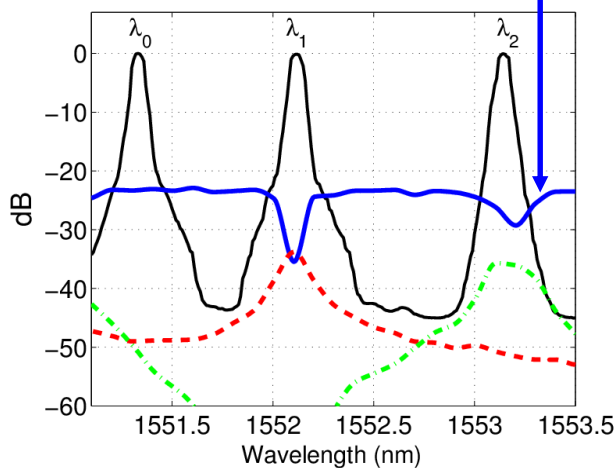
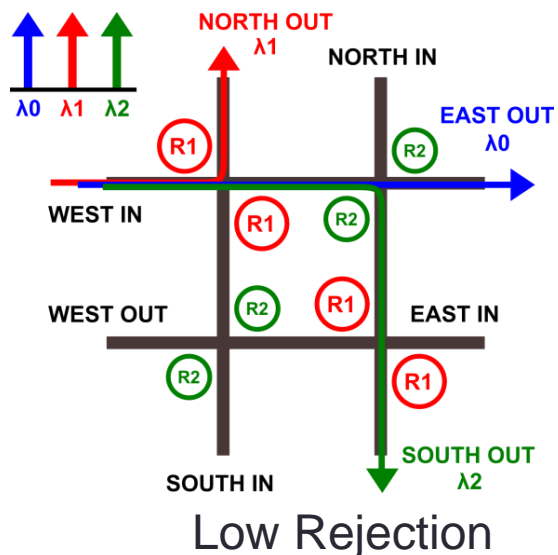


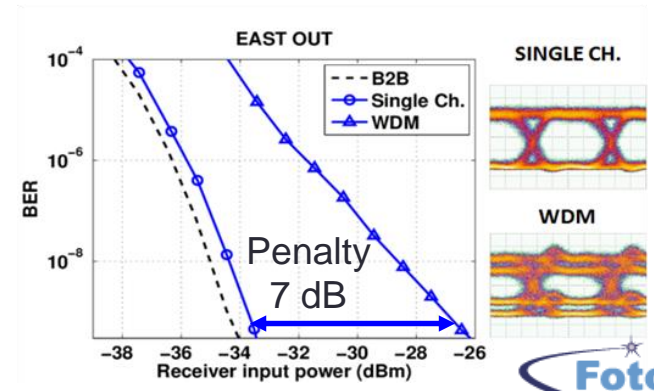
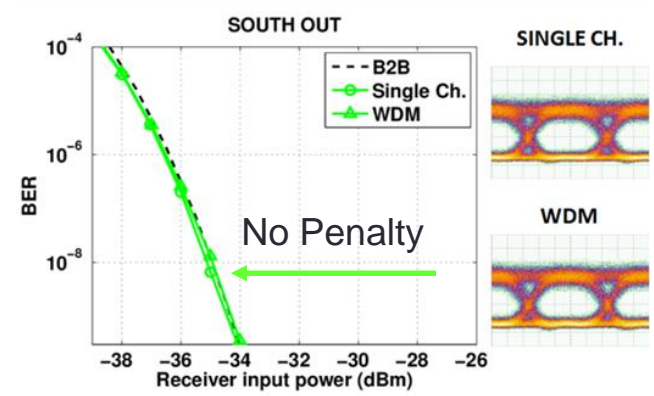
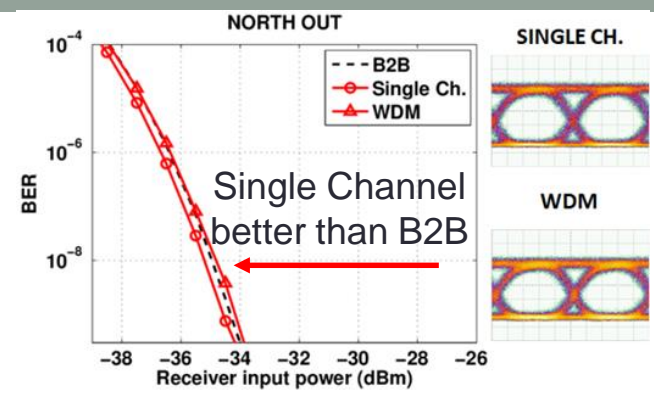
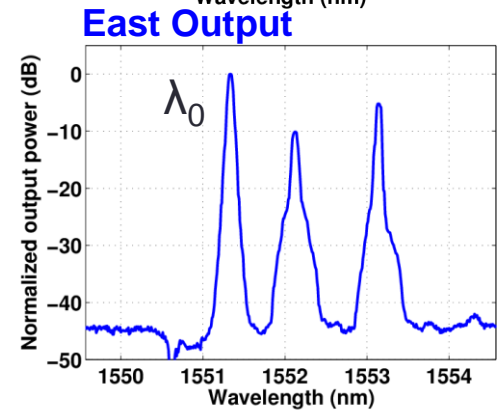
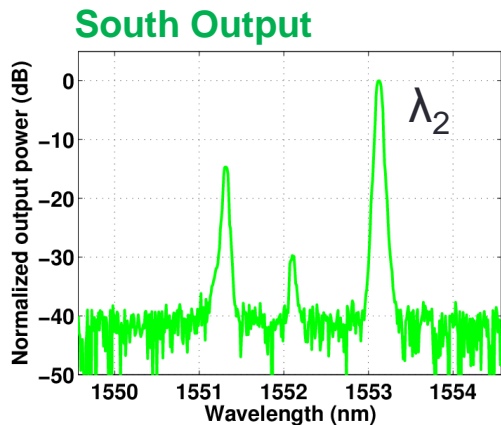
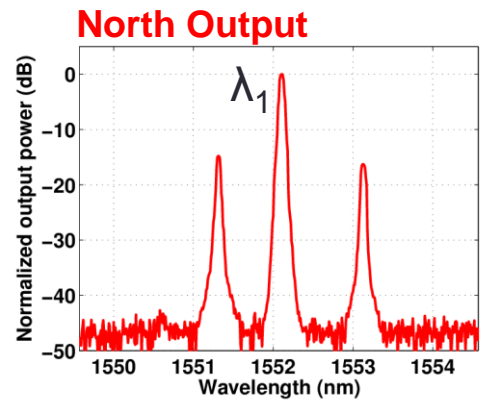
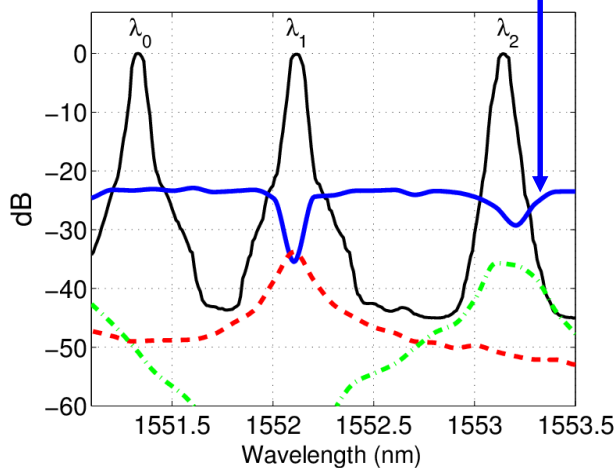
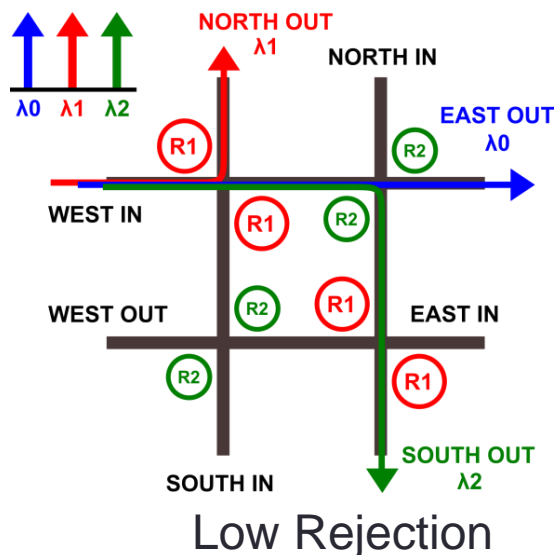
East Output



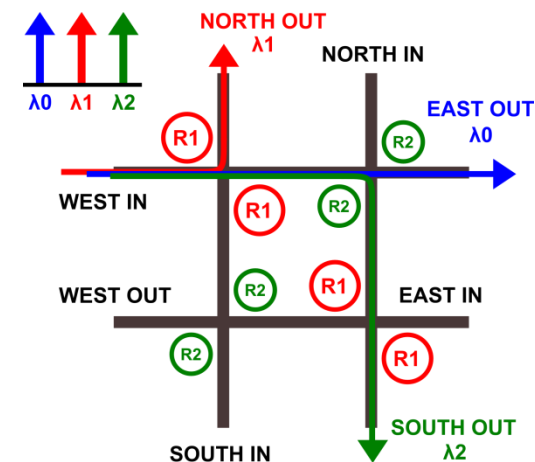








- Performance of the GWOR Router
 - Switching capabilities and robustness with respect to crosstalk demonstrated
 - BER measurements (10 Gbt/s) show
 - Fabrication issues can compromise router performances
 - 7 dB penalty on the Through Path (Low Rejection)
 - Drop-driven paths robust with respect to fabrication issues



- Sensitivity Analysis can be used to investigate the impact of technological tolerances on the performance of complex circuitry
 - The aim of Sensitivity Analysis is to assess the relations existing between a **set of input factors** subject to some **degrees of uncertainty**, and the **output(s)** of a model
- Elementary Effect (Morris Technique)
 - The Elementary Effect is the influence of a given **input factor x_i** on the **output f** of the system

$$EE_i(\mathbf{x}) = \frac{f(x_1, x_2, \dots, x_i + \Delta x_i, x_{i+1} \dots x_k) - f(x_1, x_2, \dots, x_i, x_{i+1} \dots x_k)}{\Delta x_i}$$

- The **statistical distribution of the elementary effects** (defined as F_i) is obtained by **randomly sampling N points** in the space of variation of the input factors

- The Sensitivity with respect to each parameter is measured through two quantities:

- **Mean Value of F_i**

$$\mu_i^* = \frac{1}{N} \sum_1^N |F_i|$$

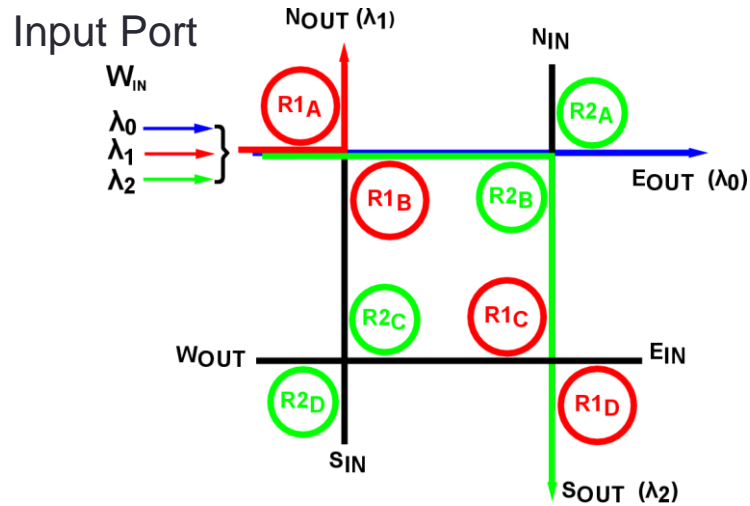
- A high value of μ_i indicates an input variable with an **important overall influence on the output**

- **Standard Deviation of F_i**

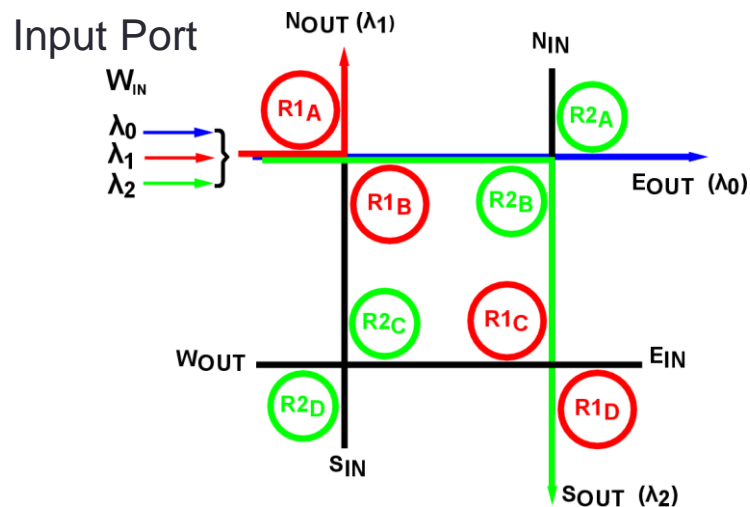
$$\sigma_i = \sqrt{\frac{\sum_1^N (F_i - \mu_i^*)^2}{N}}$$

- A high value of σ_i indicates a factor involved in **interaction with other factors** or whose effect is **nonlinear**

- Switching performance vs. variability of the rings resonances

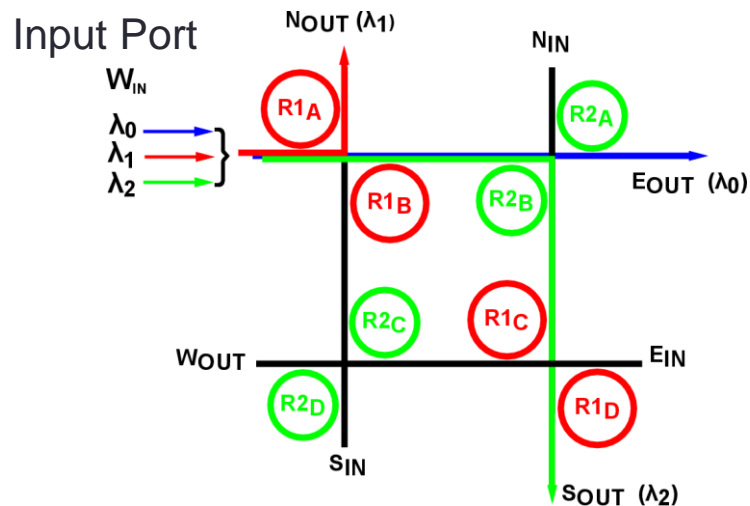


- Switching performance vs. variability of the rings resonances



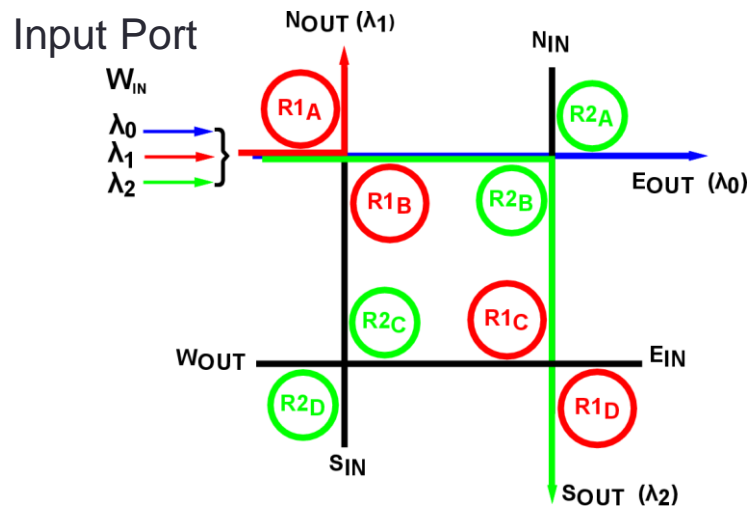
- Device behavior described through S-Parameters

- Switching performance vs. variability of the rings resonances



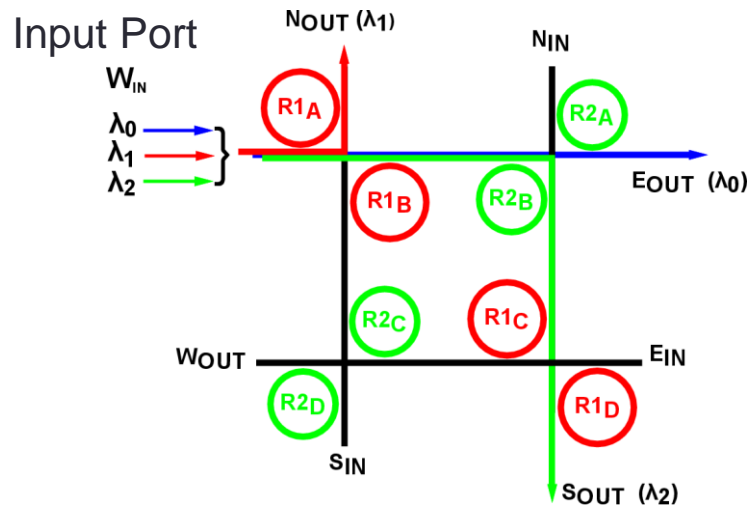
- Device behavior described through S-Parameters
- Input parameters: n_{eff} of the 8 rings

- Switching performance vs. variability of the rings resonances



- Device behavior described through S-Parameters
- Input parameters: n_{eff} of the 8 rings
- Output: signal vs noise (interference from other channels) at each output

- Switching performance vs. variability of the rings resonances

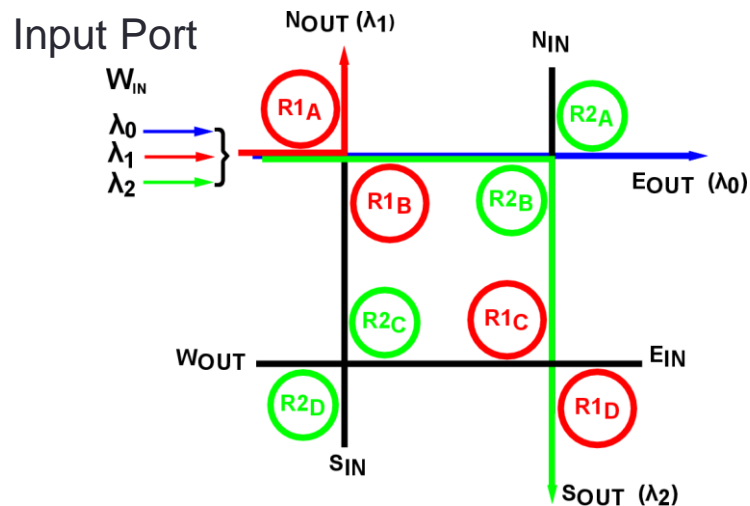


- Device behavior described through S-Parameters
- Input parameters: n_{eff} of the 8 rings
- Output: signal vs noise (interference from other channels) at each output

Channel Quality Factor (CQF) parameter

- Ratio between the power at the expected wavelength of a specific port and the power of the interfering wavelengths

- Switching performance vs. variability of the rings resonances



- Device behavior described through S-Parameters
- Input parameters: n_{eff} of the 8 rings
- Output: signal vs noise (interference from other channels) at each output

Channel Quality Factor (CQF) parameter

- Ratio between the power at the expected wavelength of a specific port and the power of the interfering wavelengths

East Output

$$CQF_0 = E_{OUT}(\lambda_0) \cdot \frac{\int_{\lambda_0-3\sigma_0}^{\lambda_0+3\sigma_0} E_{OUT}(\lambda) d\lambda}{\int_B E_{OUT}(\lambda) d\lambda}$$

North Output

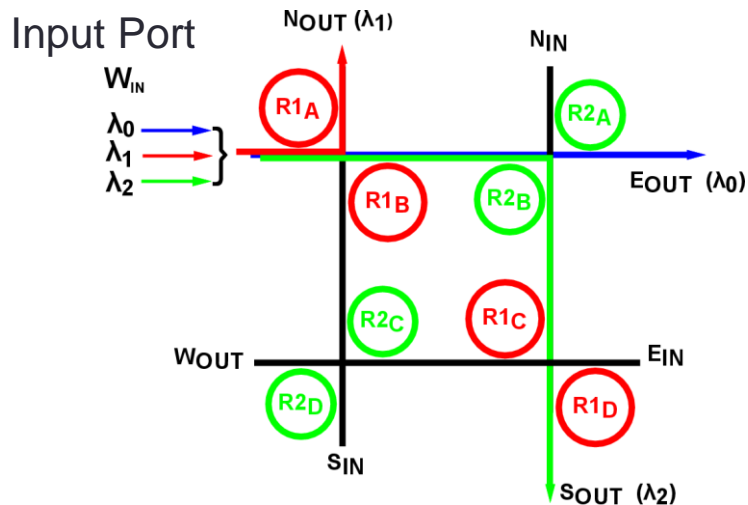
$$CQF_1 = N_{OUT}(\lambda_1) \cdot \frac{\int_{\lambda_1-3\sigma_1}^{\lambda_1+3\sigma_1} N_{OUT}(\lambda) d\lambda}{\int_B N_{OUT}(\lambda) d\lambda}$$

South Output

$$CQF_2 = S_{OUT}(\lambda_2) \cdot \frac{\int_{\lambda_2-3\sigma_2}^{\lambda_2+3\sigma_2} S_{OUT}(\lambda) d\lambda}{\int_B S_{OUT}(\lambda) d\lambda}$$

$\sigma_i = 0.0340 \mu\text{m}$ FWHM band for each carrier wavelength

- Switching performance vs. variability of the rings resonances



- Device behavior described through S-Parameters
- Input parameters: n_{eff} of the 8 rings
- Output: signal vs noise (interference from other channels) at each output

Channel Quality Factor (CQF) parameter

- Ratio between the power at the expected wavelength of a specific port and the power of the interfering wavelengths
- CQF gives an evaluation of both the finite rejection and of the detuning of the rings

$\sigma_i = 0.0340 \mu\text{m}$ FWHM band for each carrier wavelength

East Output

$$CQF_0 = E_{OUT}(\lambda_0) \cdot \frac{\int_{\lambda_0-3\sigma_0}^{\lambda_0+3\sigma_0} E_{OUT}(\lambda) d\lambda}{\int_B E_{OUT}(\lambda) d\lambda}$$

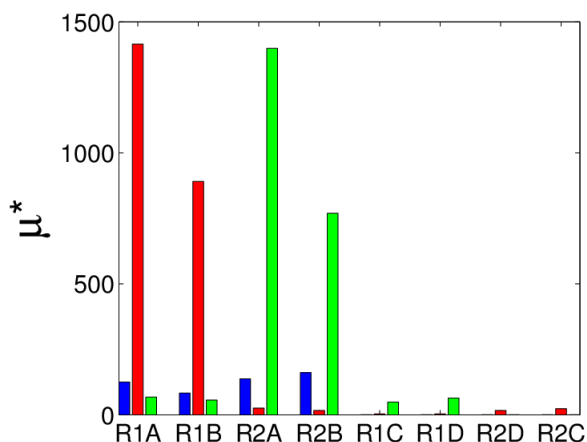
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$$CQF_1 = N_{OUT}(\lambda_1) \cdot \frac{\int_{\lambda_1-3\sigma_1}^{\lambda_1+3\sigma_1} N_{OUT}(\lambda) d\lambda}{\int_B N_{OUT}(\lambda) d\lambda}$$

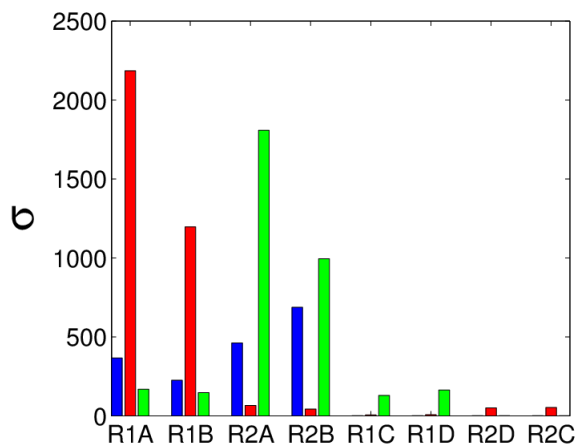
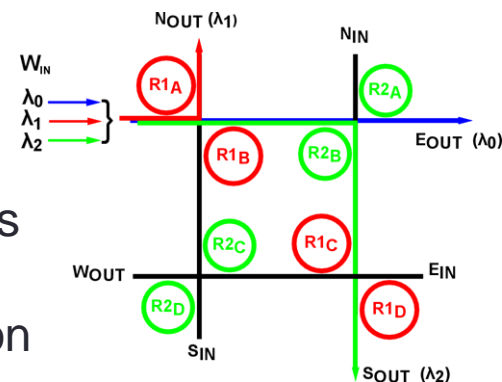
South Output

$$CQF_2 = S_{OUT}(\lambda_2) \cdot \frac{\int_{\lambda_2-3\sigma_2}^{\lambda_2+3\sigma_2} S_{OUT}(\lambda) d\lambda}{\int_B S_{OUT}(\lambda) d\lambda}$$

Rings' effective index normally distributed (mean value = nominal value) with **variance 10^{-3}**

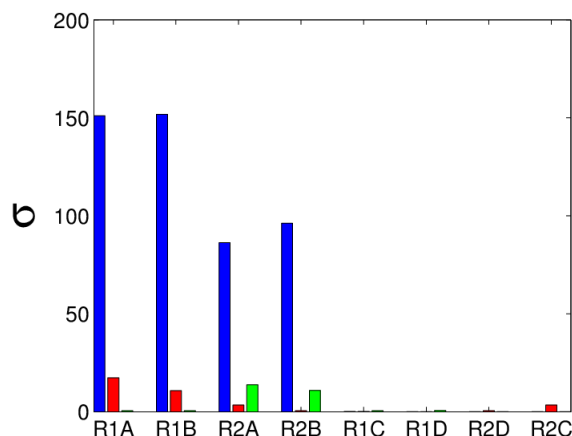
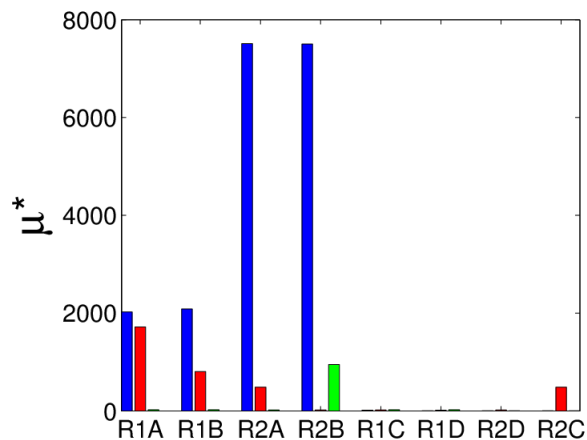


- R1A and R1B crucial rings for the **North-Out** port (red bars)
- R2A and R2B have similar effects for the **South-Out** (green bars)
- **East-Out** port less influenced (non resonant path). Effects of detuning overwhelmed by those on North and South ports

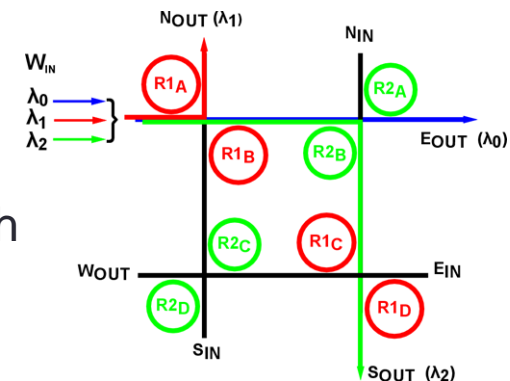


- The effects of R1A and R1B is strong on the **North-Out** port
- The same happens for R2A and R2B for what concerns the **South-Out** port
- All of these rings influence also the quality of the **East-Out** port

Rings' effective index normally distributed (mean value = nominal value) with **variance 10^{-6}**



- The most affected output is now the **East-Port**
- The rings on the **West to East** path have the greatest impact
- R1A, R1B and R2A, R2B all have a small impact (in relative terms) on the drop paths
 - The functionalities of the ports driven by the drop paths are less affected by the randomness of ring parameters
- The **West-In** to **East-Out** path is compromised
- Ring parameters variability strongly influence the switching efficiency



- Optical Network for On-Chip Optical Interconnections
 - Motivations for using ONoC
 - Basic Switching elements (1×2 PSE and 2×2 PSE)
 - 4 In - 4 Out Optical Network - GWOR
 - Problems related to fabrication tolerances
 - Performance Evaluation
 - Sensitivity Analysis as effective tool to investigate critical parameters

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Now ... Going wireless



... Optically ...



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Ferrara



ON CHIP PHOTONIC INTERCONNECTIONS: WIRED AND WIRELESS TECHNOLOGIES

Prof. Giovanna Calò, Politecnico di Bari

Prof. Gaetano Bellanca, University of Ferrara

Contacts: giovanna.calo@poliba.it, gaetano.bellanca@unife.it

OUTLINES

- Introduction
- Design of on-chip integrated antennas
 - Plasmonic antennas
 - Antenna arrays
- Wireless link performance
 - Finite Difference Time domain simulations
 - Ray tracing simulations
 - Bit Error Probability

The WiNOT Project

- **W**ireless **N**etworks through on-chip **O**ptical **T**echnology
- Italian National Project
- Starting date: December 2017
- 3 Universities Involved
 - **Politecnico di Bari** (Coordinator): design of optical antennas
 - **University of Bologna**: development of a ray-tracing tool to investigate the optical propagation inside the chip
 - **University of Ferrara**: network analysis and optimization. Measurements on fabricated devices
- Technological Partner
 - IIT - Center for Biomolecular Nanotechnologies



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The WiNOT Project

Design of Optical Antennas for Wireless Optical Connections

Development of a Ray-Tracing Simulator to investigate propagation in Complex Environments

Network Analysis Optimization

Antenna Design

Fabrication

Integration with the Optical Layer

Antenna Array

Measurements

Long - Distance FDTD Simulations

Ray - Tracing Simulator

Network performance with a single link

Network performance with multiple links

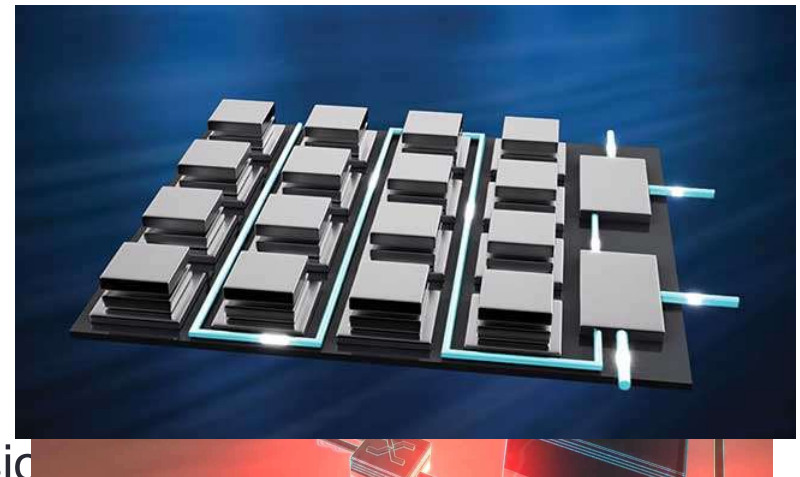
Performance evaluation and Optimization



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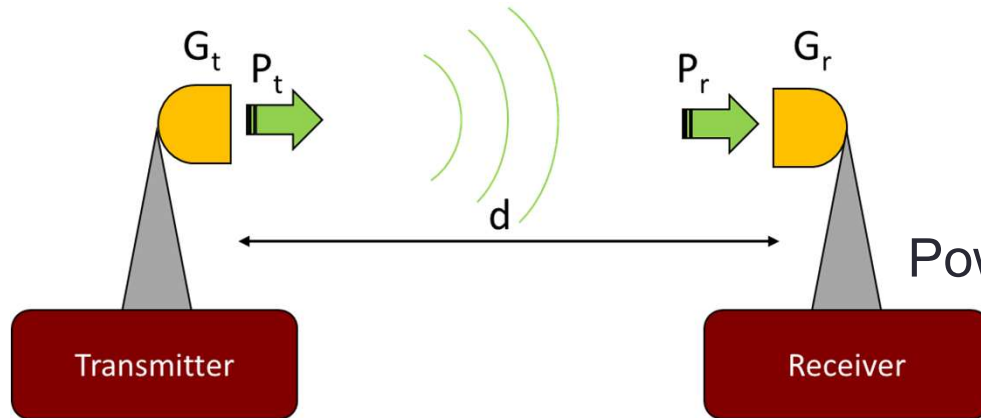
Introduction

- Optical Interconnections on-chip proposed to have efficient communication between processors on the same die (ONoC)
 - Problems: footprint, layout complexity, signal loss and crosstalk due to multiple waveguide crossing
- RF Wireless Connections (WiNoC) investigated, to avoid multiple waveguide crossing
- Optical Wireless NoC (OWiNoC)
- All-Optical solution(Wired + Wireless) presenting some advantages
 - No transceivers
 - No latency (for optical-to-electrical conversion)
 - Bit transparency
 - Reduced power consumption



Wireless Optical Network on Chip

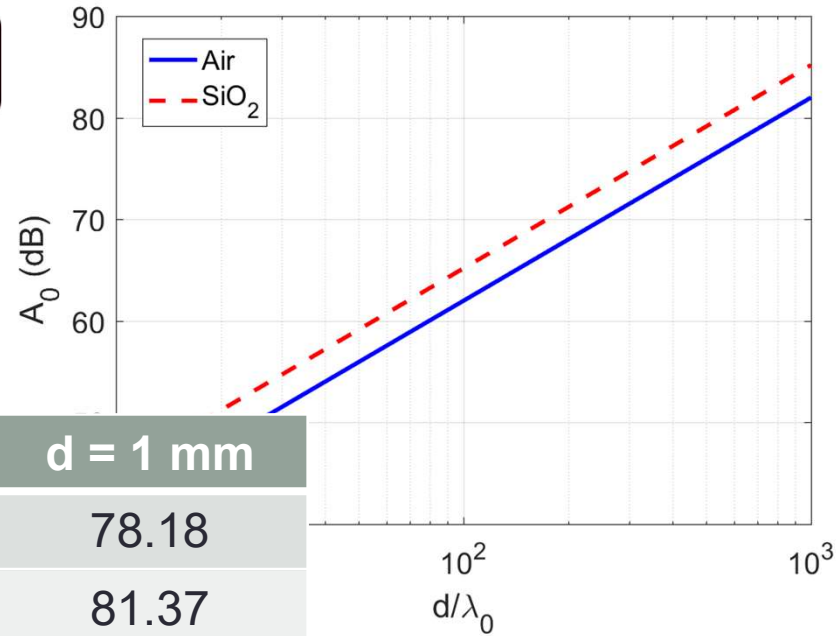
- Propagation in homogeneous medium: the Friis formula



$$A_0 = -20 \log_{10} \left(\frac{\lambda_0/n}{4\pi d} \right)$$

Power decay for free-space propagation

$$P_r = P_t + G_r + G_t + 20 \log_{10} \left(\frac{\lambda_0/n}{4\pi d} \right)$$



P_r : received power (dBm)

$\lambda_0 = 1.55 \mu\text{m}$	$d = 50 \mu\text{m}$	$d = 100 \mu\text{m}$	$d = 1 \text{mm}$
A_0 - Air	52.16	58.18	78.18
A_0 - SiO ₂	55.35	61.37	81.37

λ_0 : wavelength

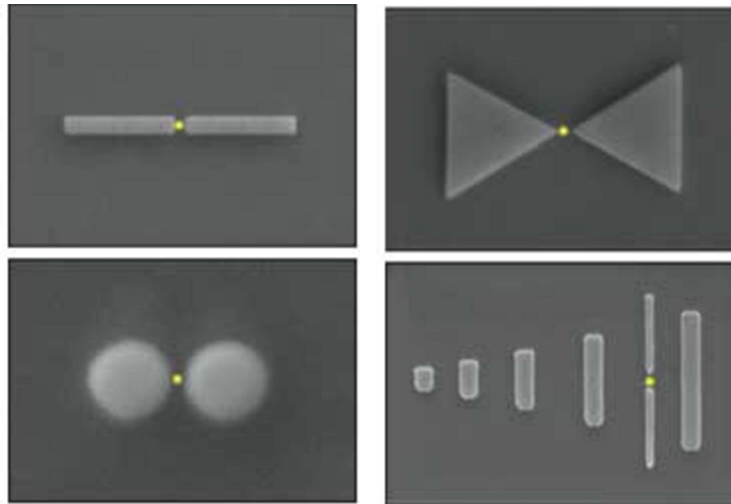
n : refractive index

d : distance of the link

$P_t = 0 \text{ dBm}$ (1mW), $P_r = -20 \text{ dBm}$, $A_0 \cong 82 \text{ dB} \Rightarrow$
 \Rightarrow OWiNoC applications need antennas with high gain

Antennas for Optical Wireless Network on Chip

- Plasmonic Optical Antennas



- Problems

- Directivity is not very high
- Resonant antennas \Rightarrow
 - \Rightarrow Small bandwidth
- Excitation through silicon optical waveguides challenging

<https://www.photonics.ethz.ch/en/general-information/research/optical-antennas.html>

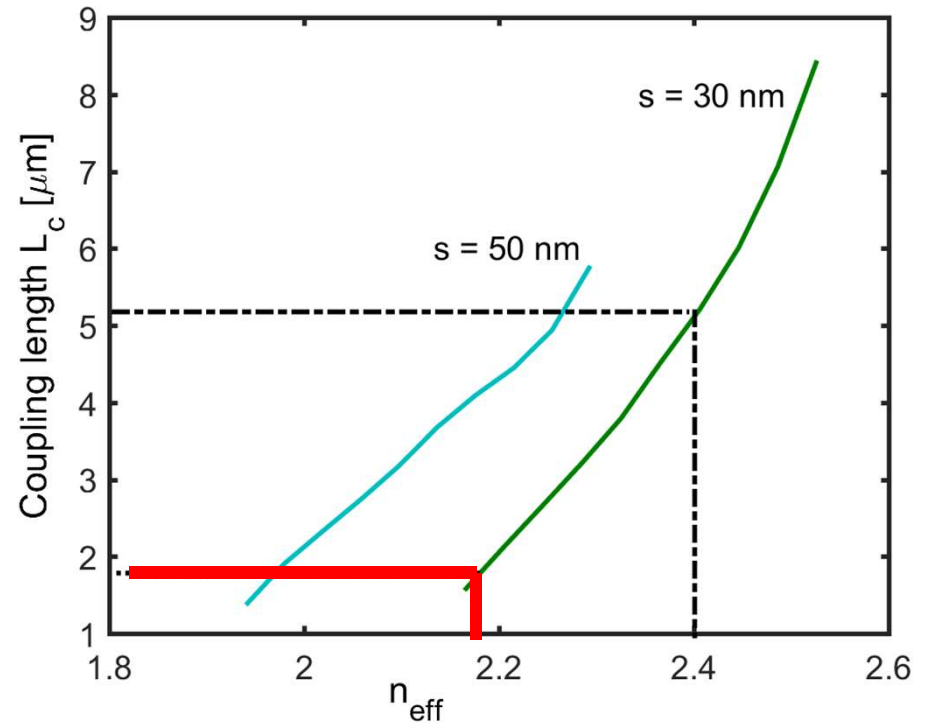
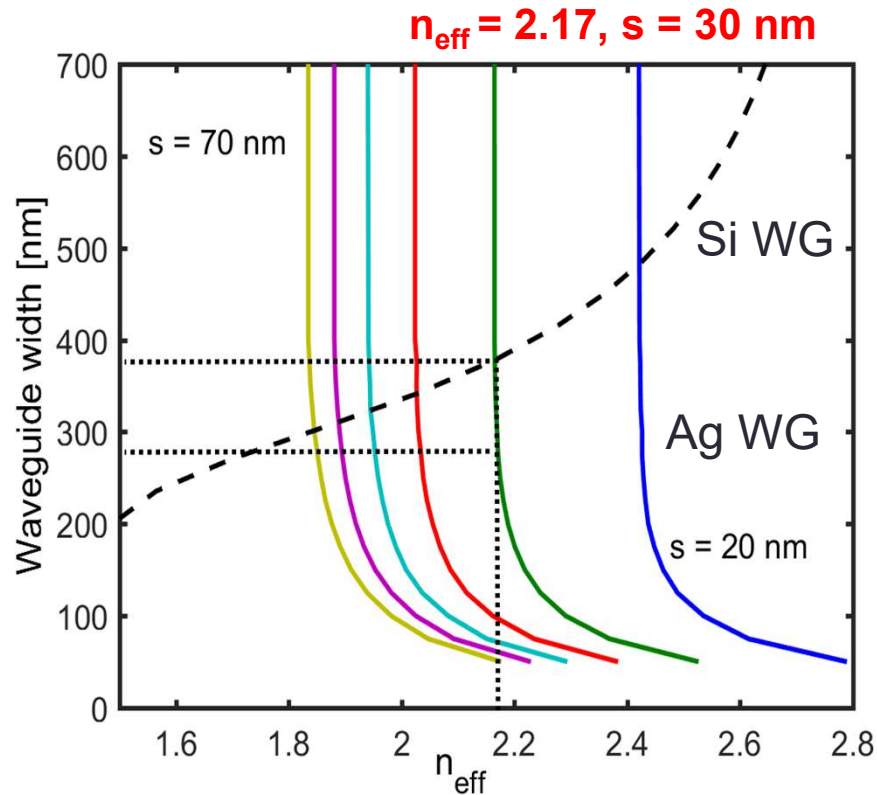
- Vivaldi Antenna

- Used in the microwave range
- High gain and large bandwidth



- **Design of a Vivaldi Antenna for Optical Wavelengths**

Vivaldi plasmonic antenna



Coupled Mode Theory

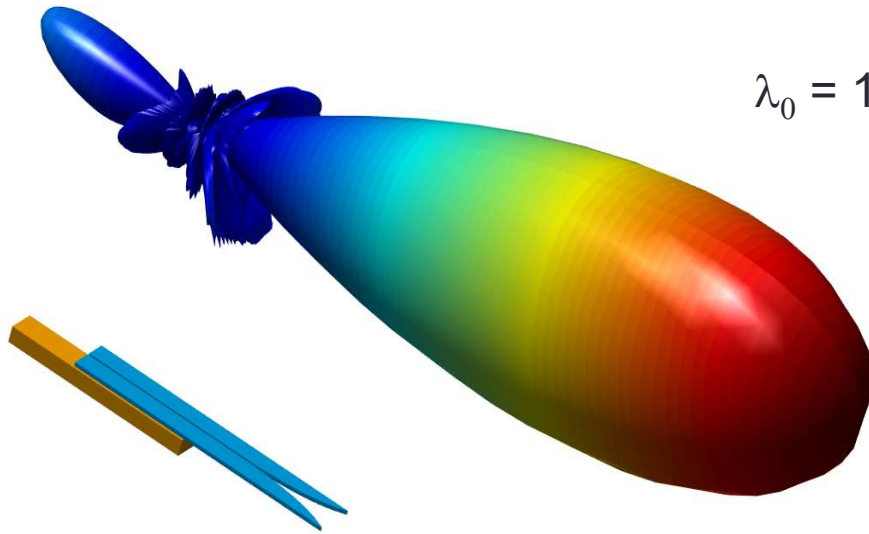
Efficient coupling: Silicon and Plasmonic waveguides with same n_{eff} for their fundamental (TE) modes

$$L_c = \frac{\lambda_0}{2|n_e - n_o|}$$

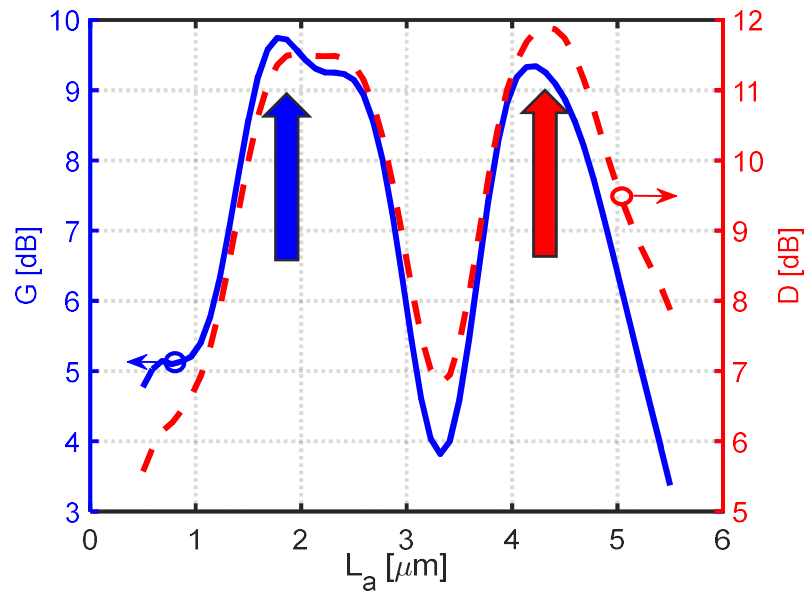
$s = 30 \text{ nm}, n_{\text{eff}} = 2.17, w = 380 \text{ nm}, p = 270 \text{ nm}, L_c = 1.63 \mu\text{m}$

[1] G. Bellanca et al., Optics Express (2017)

Vivaldi plasmonic antenna

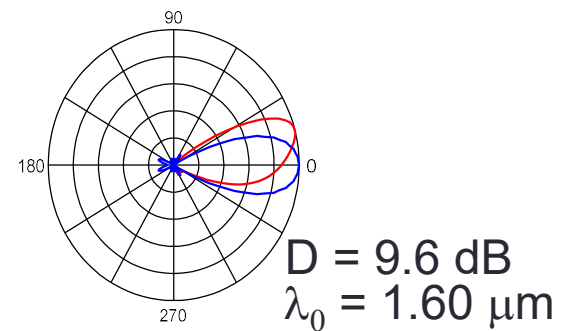
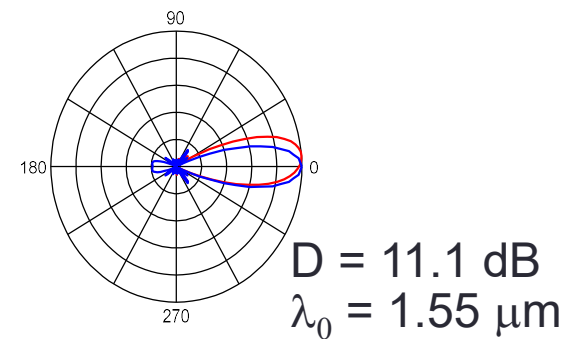
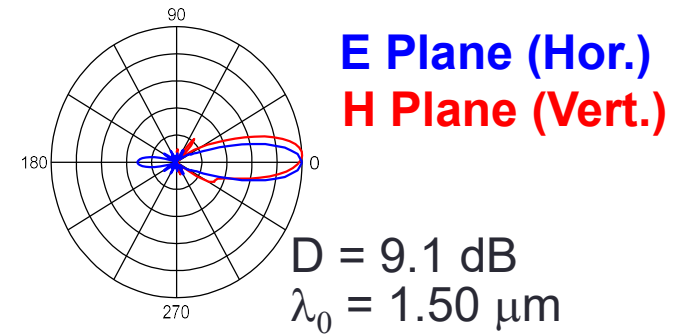


$\lambda_0 = 1.55 \mu\text{m}$



Optimized Geometry: $L_a = 1.75 \mu\text{m}$

Directivity



Optimized Optical Vivaldi Antenna

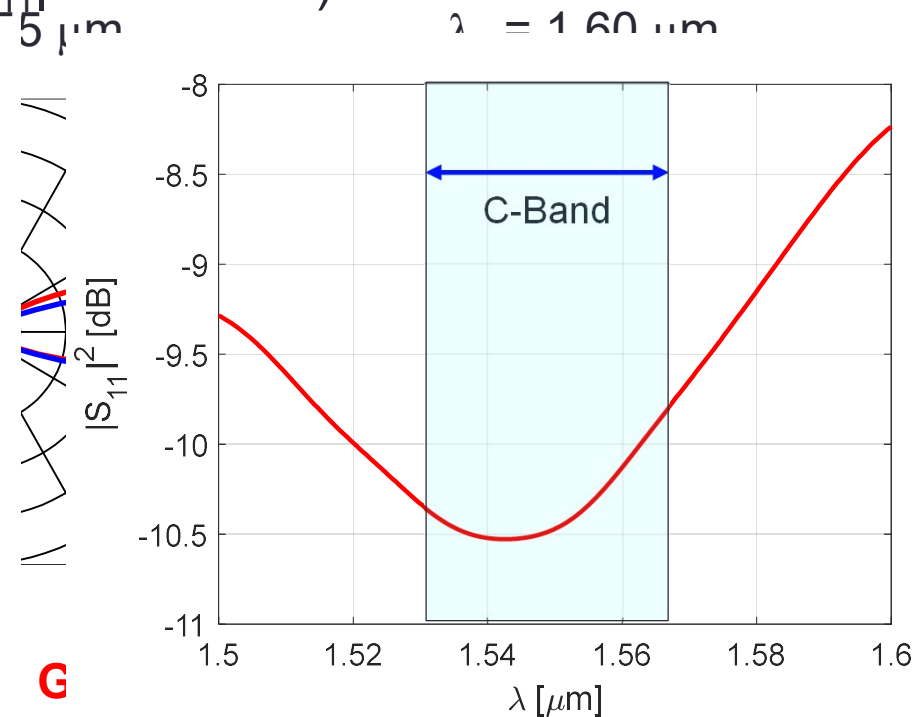
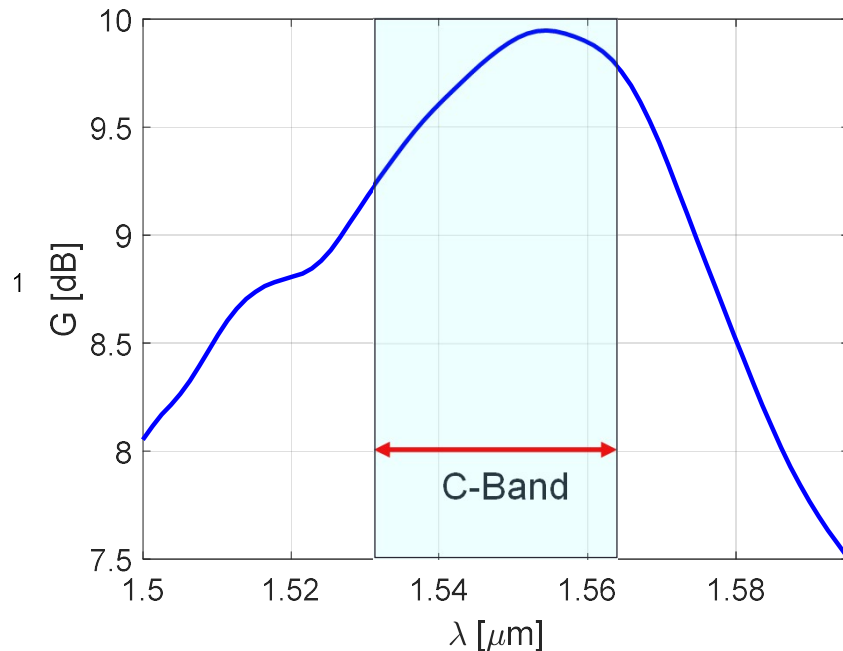
- Coupler length L_c , Antenna length L_a and Antenna shape have been optimized to maximize Gain and Bandwidth
- The Vivaldi antenna performs well for all the wavelengths in the C Band (1530 ÷ 1565 nm)
 - Radiation patterns have regular shapes

E Plane (H)

H Plane (V)

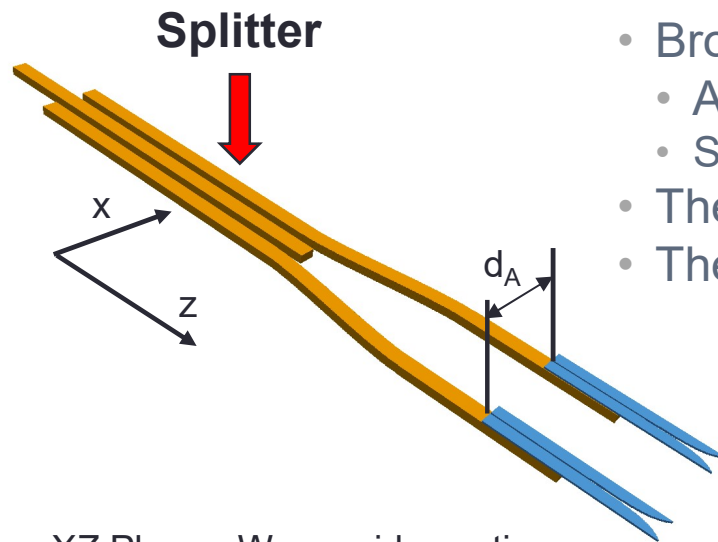
• Gain always above 9 dB

• Impedance Matching is good ($|S_{11}|^2 < -9.5$ dB)



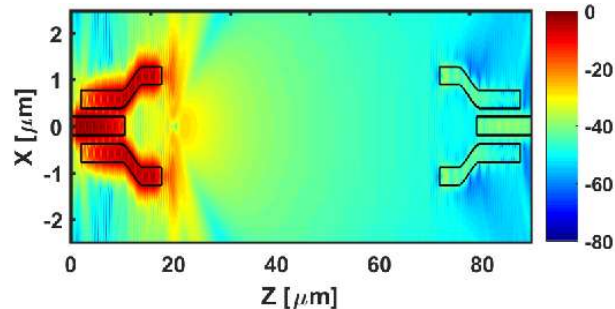
Broadside array of two Vivaldi radiators

- Antenna Arrays are compositions of Antennas suitably positioned and properly excited (playing with both amplitude and phase)
 - Directivity increase
 - Beam-Steering (changing the direction of the main lobe)

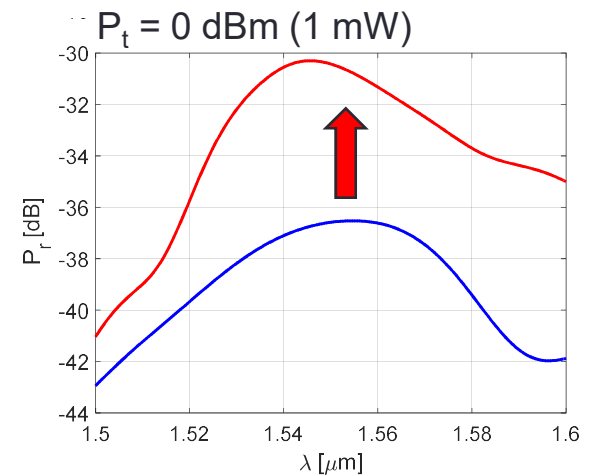
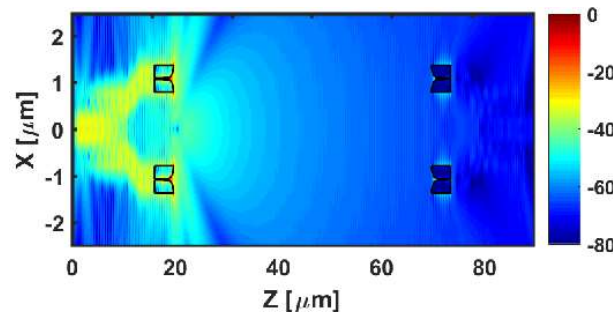


- Broadside Array of Vivaldi Antennas
 - Antennas aligned along the x axis
 - Same Amplitudes and Phases of the Excitations
- The Gain increases of about 3 dB
- The Received Power increases of about 6 dB

XZ Plane - Waveguide section



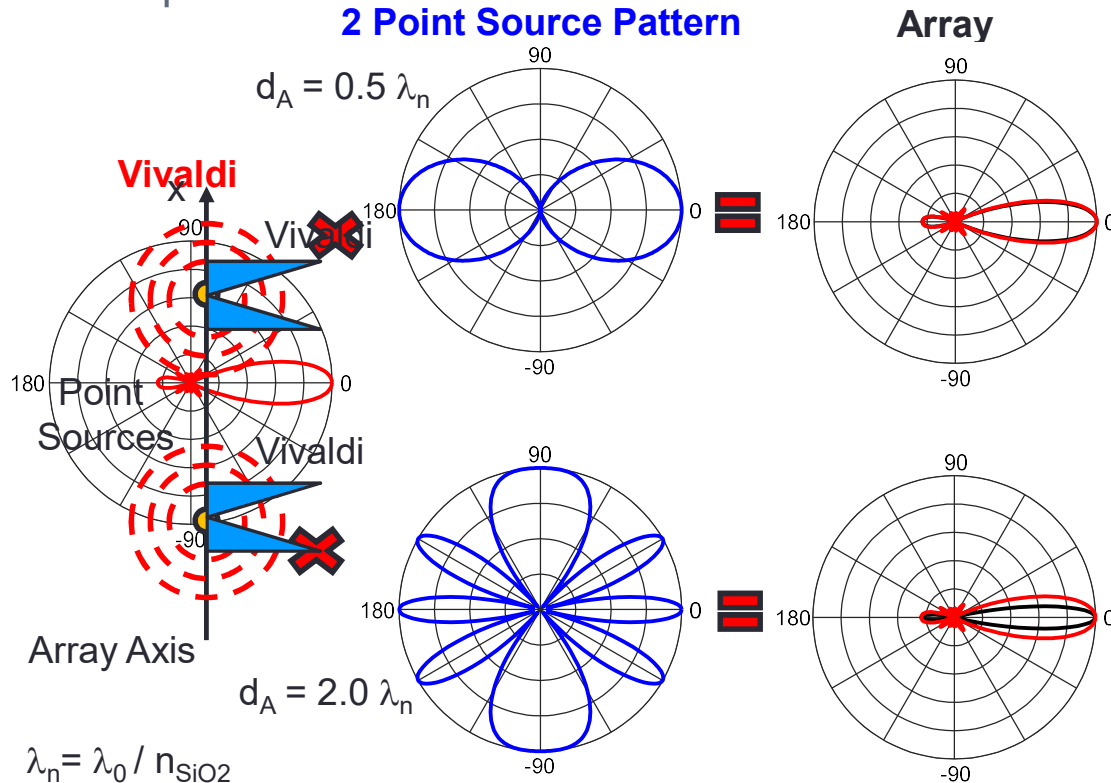
XZ Plane - Antenna section



[2] G. Calò et al., *Optical and Quantum Electronics* (2017)

Broadside array of two Vivaldi radiators

- Radiation Pattern of the Array obtained through pattern multiplication theorem
 - Pattern of elementary (point) sources
 - Pattern of the Vivaldi Antenna
 - With the proposed configuration, only radiation patterns on the Horizontal (E) plane can be modified



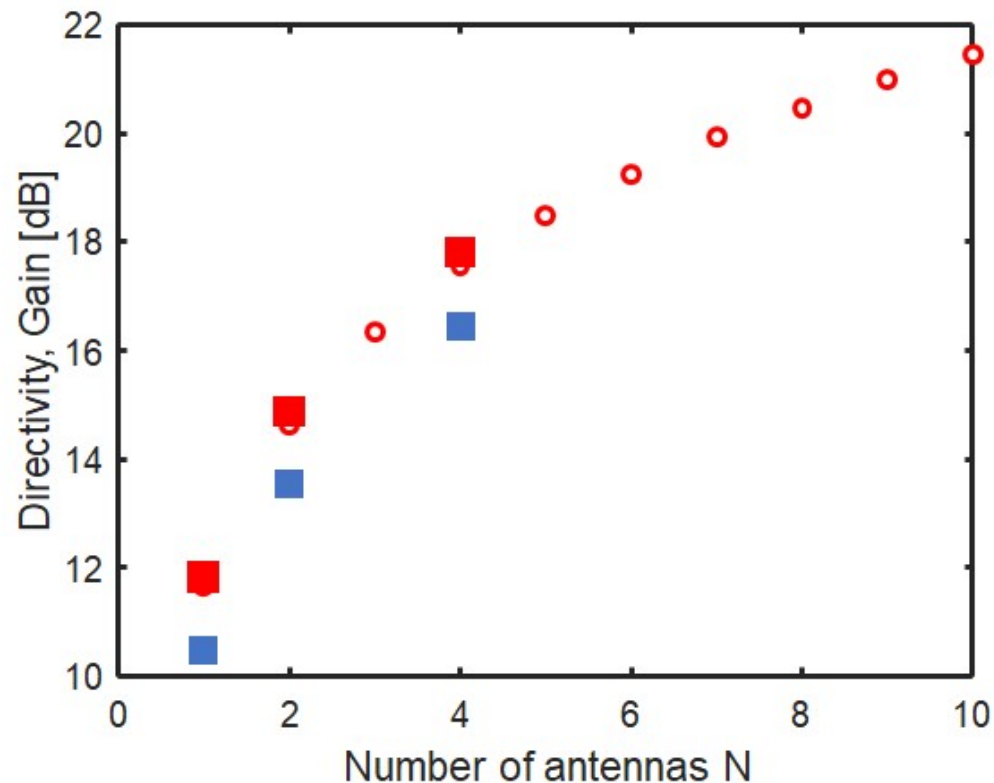
No Grating Lobes on the Radiation Pattern of the 2 Point Source
 Radiation Patterns of Array and Vivaldi almost indistinguishable
 No increase in the directivity

Grating Lobes on the Radiation Pattern of the 2 Point Source
 Narrower Radiation Pattern for the Array
 \Rightarrow Increase in the directivity ($D = 16.7$ dB)

Radiation Pattern Vivaldi Antenna
 Radiation Pattern Array of Vivaldi Antennas

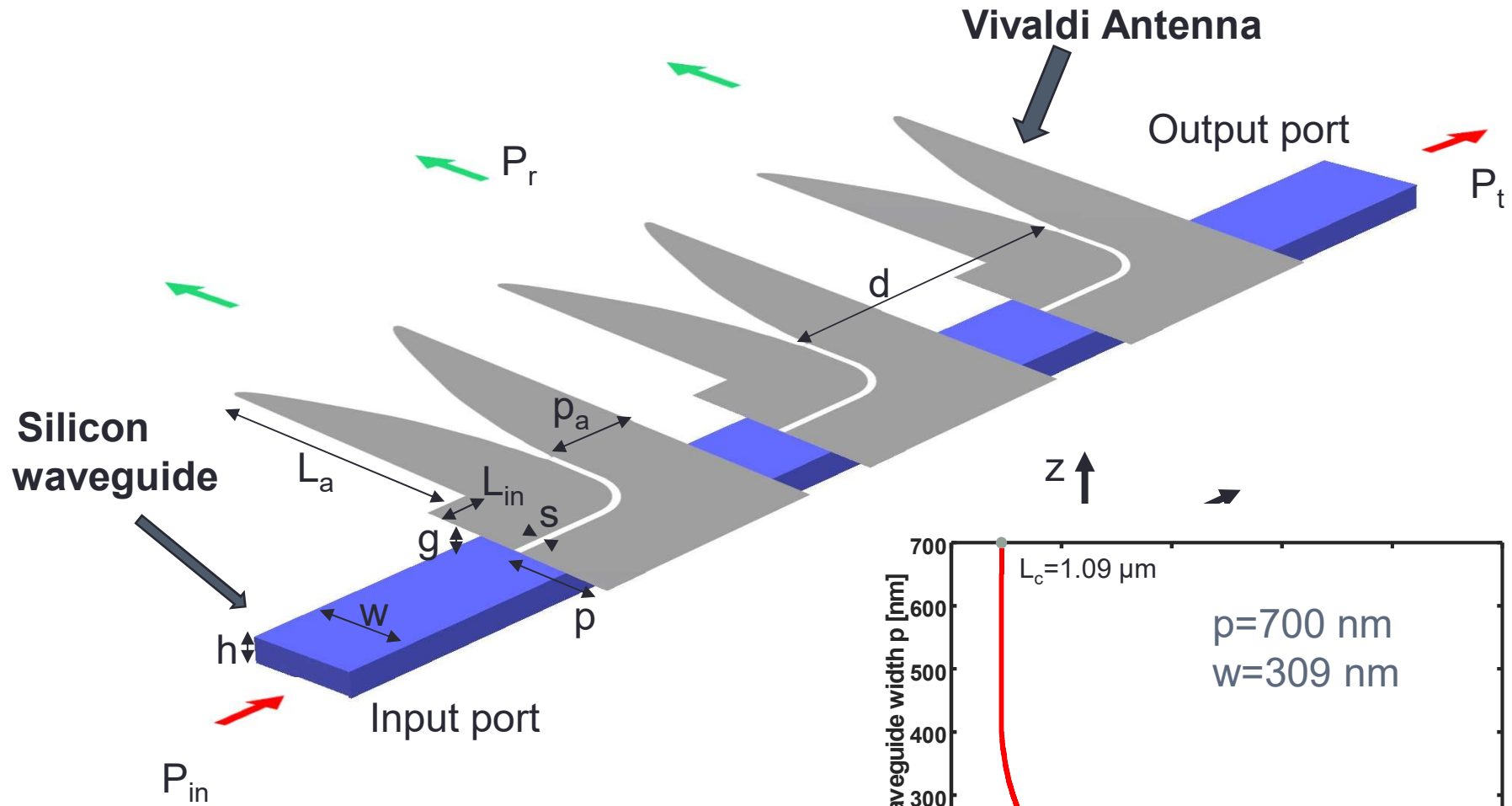
Radiation Patterns on the Horizontal Plane

Broadside array of N Vivaldi radiators



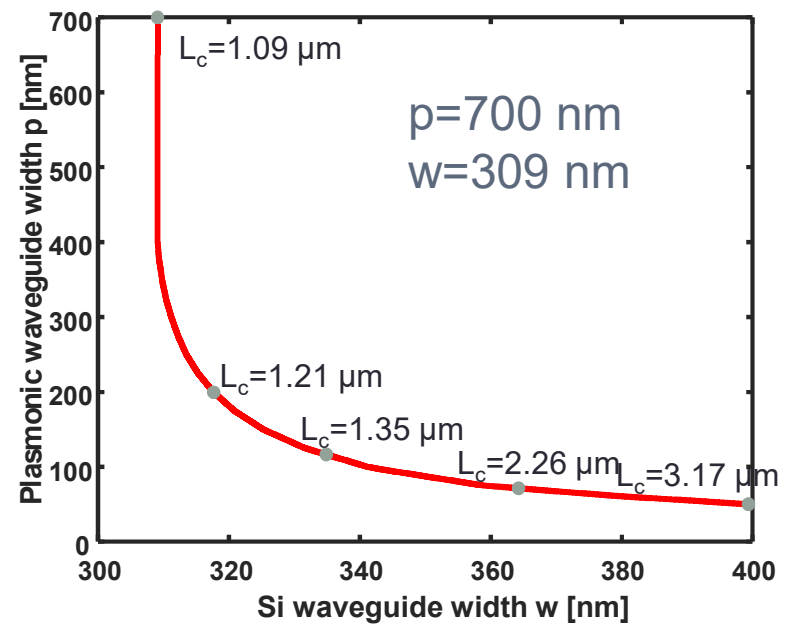
- Array directivity (red squares) and gain (blue squares) as a function of the number of antenna N (N=1, 2, and 4) by FDTD. The red circles report the array directivity calculated according to antenna theory
- In all the considered cases, the radiation efficiency is $\eta = G/D = 0.7$
- Large footprint of the overall array owing to the feeding network.

Travelling wave Vivaldi antenna array



$s=60$ nm, $g=80$ nm, $h=220$ nm

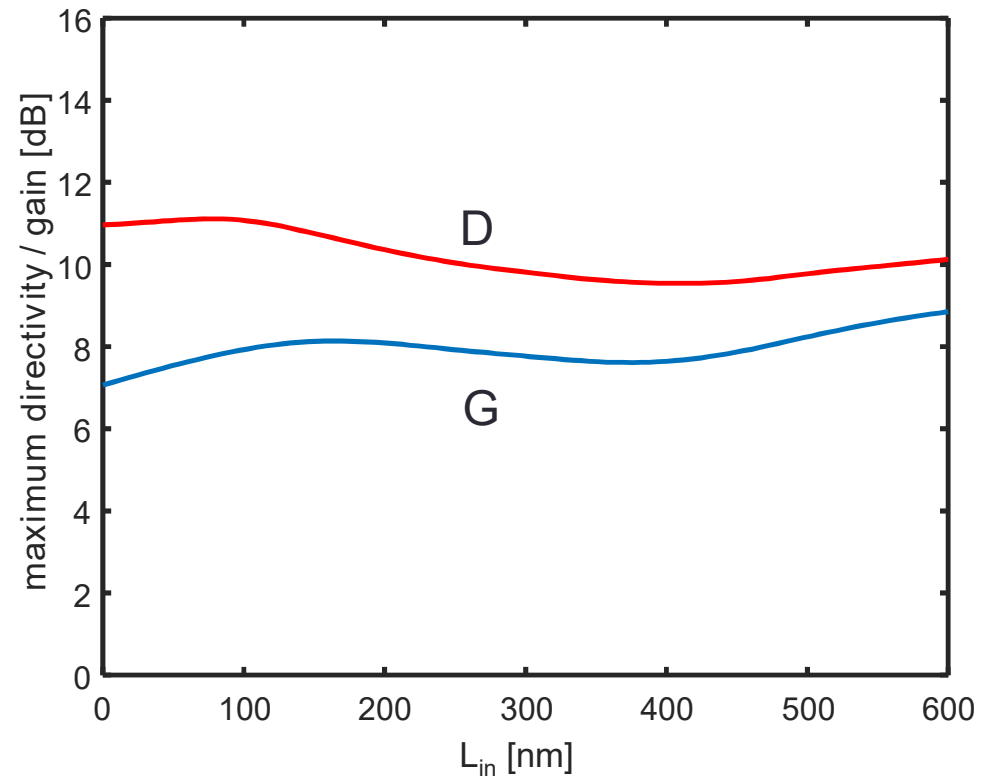
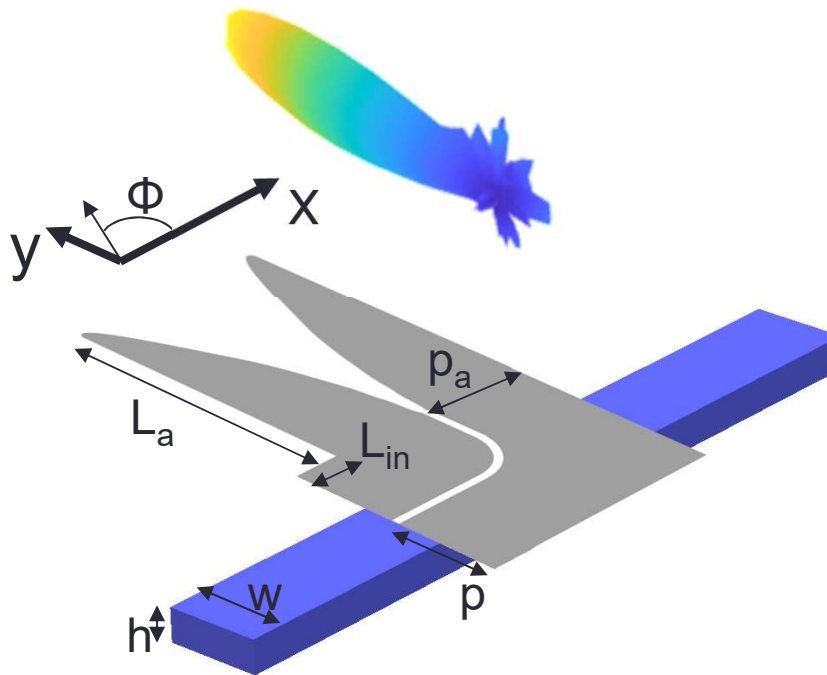
Cross section designed through the CMT



Design of the tilted Vivaldi antenna

- Design requirements for the single antenna: **partial power transfer** from the Si to the plasmonic slot waveguide, as well as **good antenna directivity**

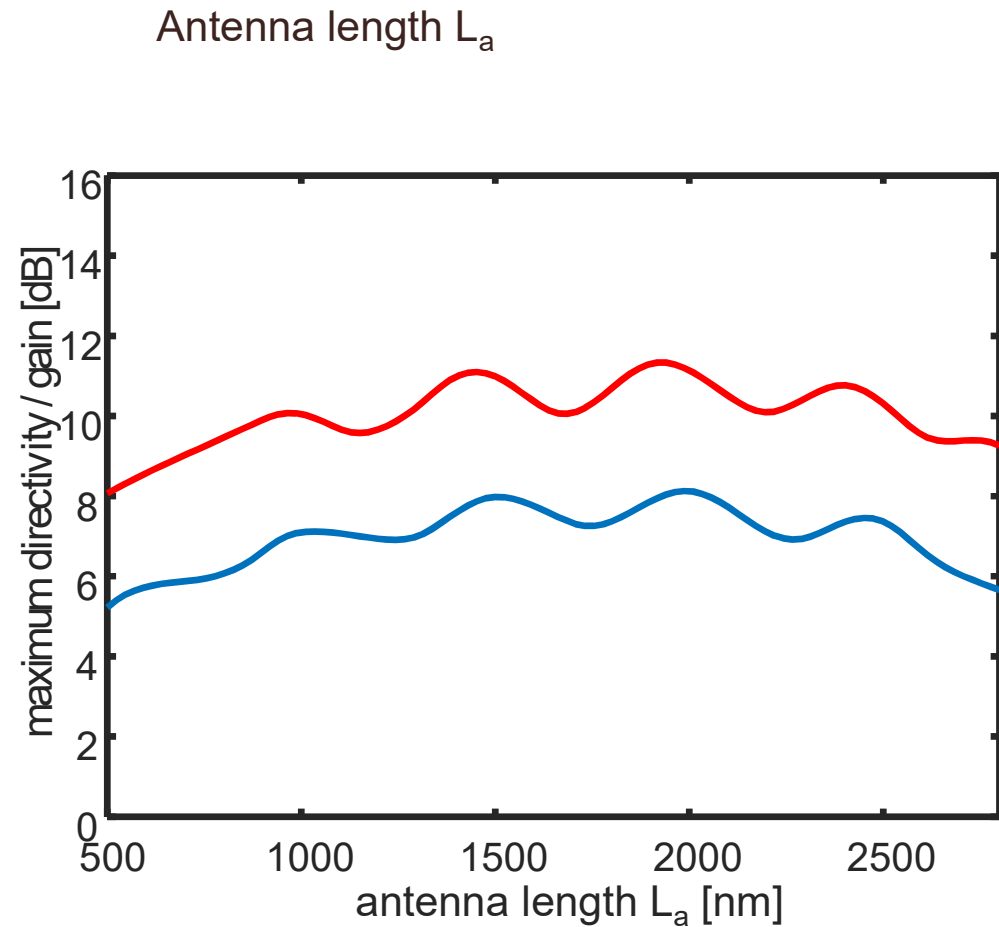
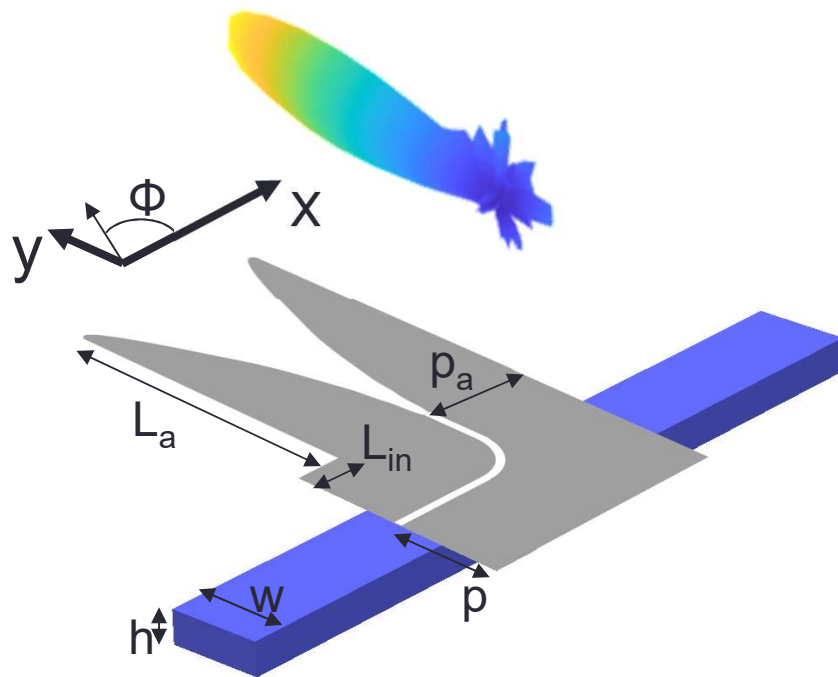
Length of the input straight region L_{in}
(antenna length $L_a=1500$ nm, arbitrarily chosen)



$L_{in}=100$ nm, maximum directivity $D=11.1$ dB and enough power left in the Si waveguide to feed the following antennas

Design of the tilted Vivaldi antenna

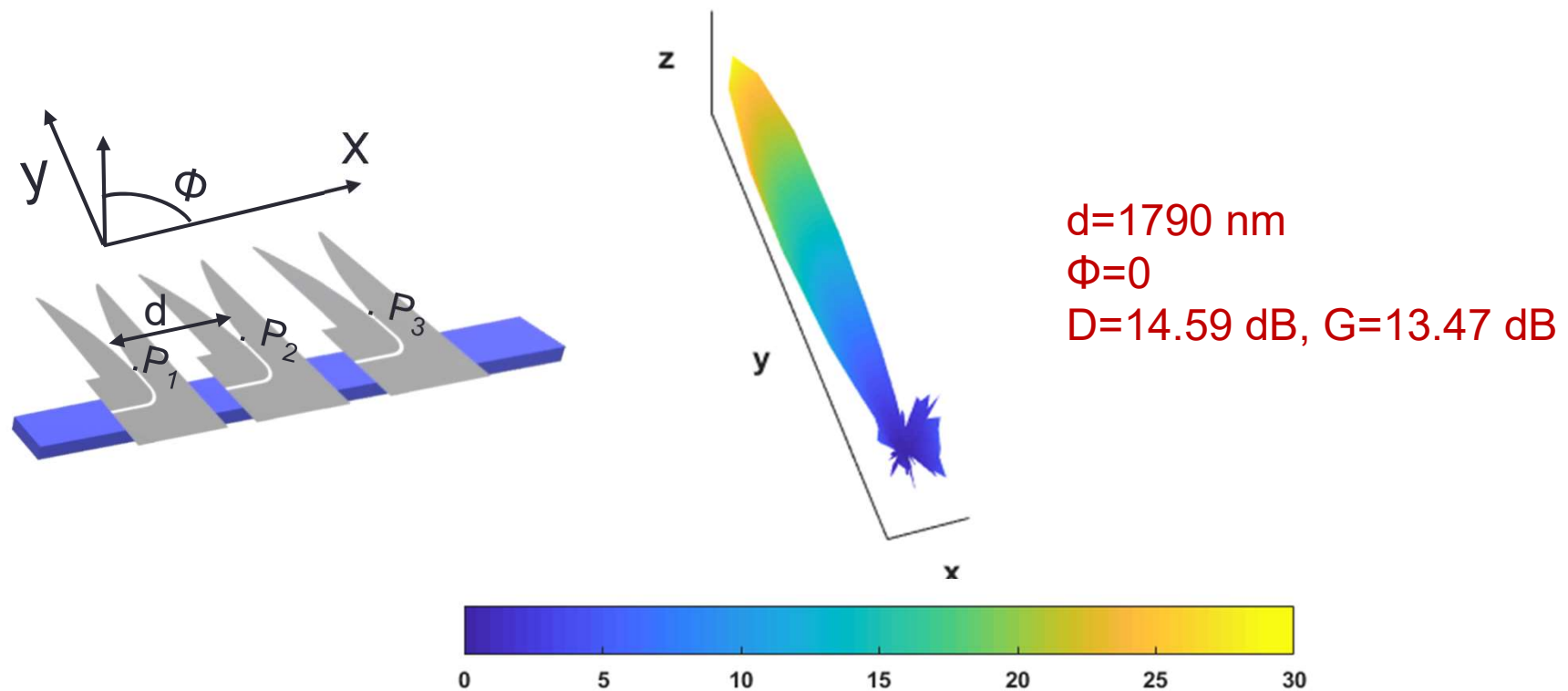
- Design requirements for the single antenna: **partial power transfer** from the Si to the plasmonic slot waveguide, as well as **good antenna directivity**



$L_a=2000$ nm, maximum directivity $D=11.4$ dB

Tilted Vivaldi antenna ARRAY (N=3)

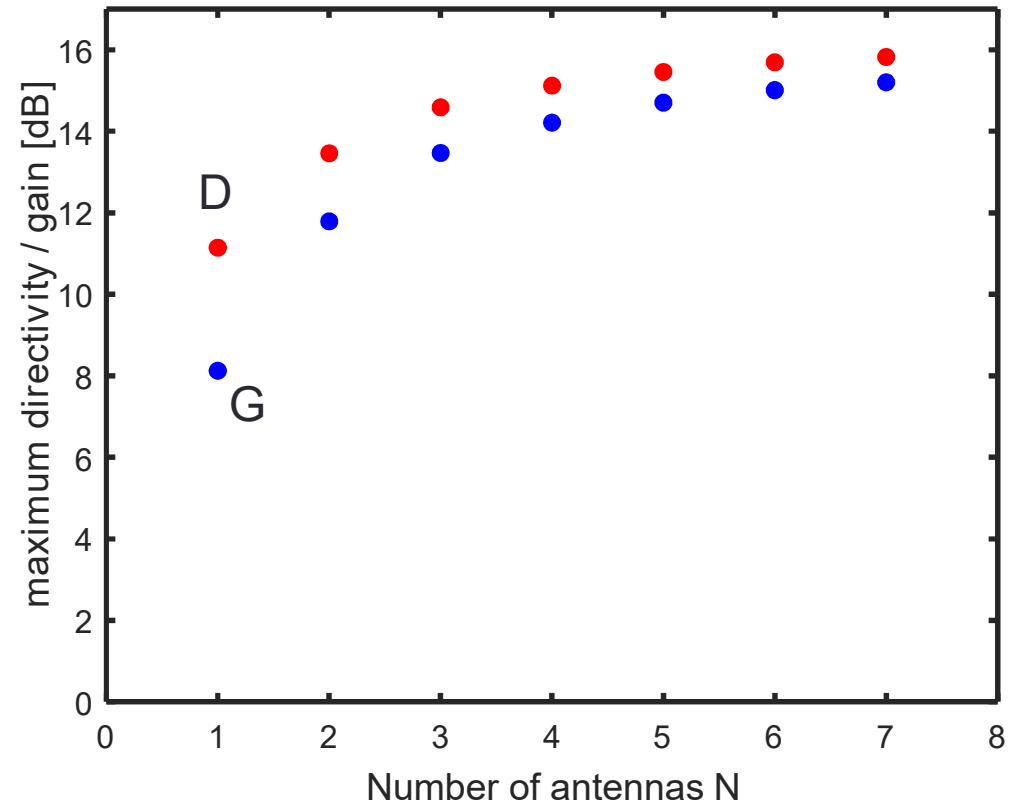
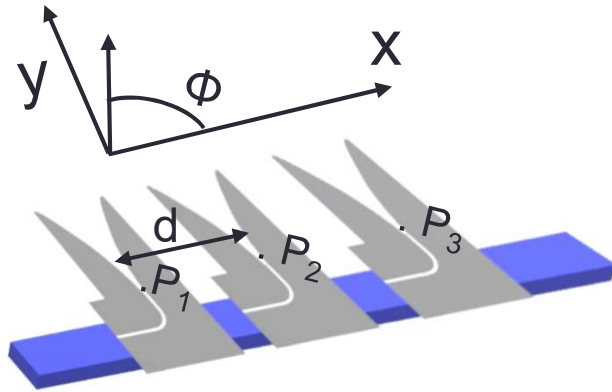
- The variation of the distance between the antennas induces a phase shift between the antennas



variation of the directivity and of the gain with d
variation of the tilt angle Φ of the beam with d

Tilted Vivaldi antenna ARRAY

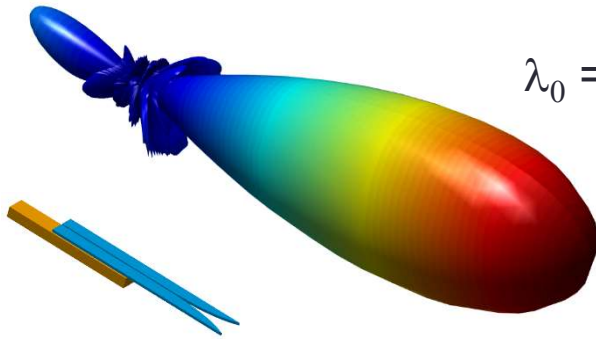
- Gain and directivity increase with the number of antennas



$N=5$, $d=1790$ nm, $\Phi=0$
 $D=15.46$ dB, $G=14.70$ dB

Conclusions

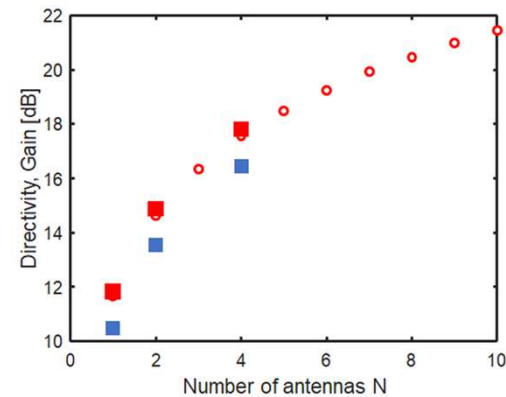
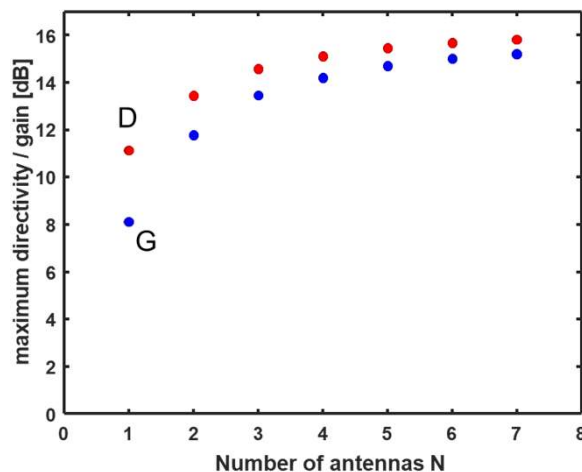
- On-Chip Optical Wireless Connections: High Gain antennas are needed to cope with free space attenuation



$$\lambda_0 = 1.55 \mu\text{m}$$

- Vivaldi Antenna:
Coupling with SOI waveguides
9.9 dB Gain – Full C Band coverage

- ❖ Broad-side antenna arrays:
High directivity (N=5, D=18 dB)
large footprint (tens of μm)



- ❖ Travelling wave antenna arrays:
lower directivity (N=5, D=15 dB)
small footprint ($3.5 \mu\text{m} \times 8.7 \mu\text{m}$)